Adaptive Nonparametric Approach for Guaranteed Real-Time Detection of Targeted Signals in Multichannel Monitoring Systems

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Abstract—An adaptive nonparametric method is proposed for stable real-time detection of seismoacoustic sources in multichannel C-OTDR systems with a significant number of channels. This method guarantees upper boundaries for probabilities of Type I and Type II errors. Properties of the proposed method are rigorously proved. The results of practical applications of the proposed method in a real C-OTDR-system are presented in this report.

Keywords—Adaptive detection, change point, interval estimation, guaranteed detection, multichannel monitoring systems.

I. INTRODUCTION

Monitoring systems for control of super-extended objects (oil & gas pipelines, railways, national borders) are always multichannel complexes without exception. It is true for brand new C-OTDR monitoring systems [1]-[4] as well as for convenient large-scale monitoring multi-point sensor systems (seismic braids etc.). At different times and different places the conditions of observation are dramatically different. These circumstances influence sensors systems very strongly. The influence implies an increase in Type I and Type II errors. While noise level may be dramatically different in various time intervals for one and the same channel, the industrial noise power and its spectral characteristics as a rule are stable for extended periods of time (no less than a few minutes or sometimes even hours). Unlike the industrial noises, targeted signals have high power and short duration (no more than a few minutes). So, targeted signals have a shorter stability period with respect to stability period of noises. Using this assumption we can build an adaptive real-time detector which will guarantee prescribed level for Type I and Type II errors. That approach will be described in this paper on an example of C-OTDR monitoring system with a high number of channels (more than 20,000).

II. STATEMENT OF THE PROBLEM

Let us assume that we have a multichannel monitoring system. There are array of statistically independent channels, which are used for getting targeted signals. Indexes of system channels in conjunction form a set \( Z = \{1,2,...\} \). Observations are made at successive times, which form a set \( T = \{t_1,t_2,...\} \), \( \forall i > 0: t_i - t_{i-1} = \Delta t > 0 \) thus, the observations are

\[ S_j(t) = \{S_j(t)|t \in T\}. \]

Let us denote:

1. \( \tau_j \) is random moment time, \( \tau_j \in T \). So, \( \tau_j \) is the moment of abrupt change of the observations distributions in \( j \)-th channel. This change happened due signal appearance. Actually, \( \tau_j \) is the change-point moment [5], [6] of observation distributions.
2. \( t_0 \) is time of observation start;
3. \( h \) is the sample size for adaptation to noise (this parameter is selected a priori);
4. \( P_r \) - confidence coefficient, \( 0 < P_r < 1 \);
5. \( \Delta(k) = 2((1-P_r)k)^{\alpha}\); (hypothesis \( H_0 \): in channel do not signal (background model);
6. hypothesis \( H_1 \): in channel is signal (signaling model);
7. \( \alpha \in [0,\alpha] \) is a predetermined upper bound for the probability of making type I errors;
8. \( \beta \in [0,\beta] \) is a predetermined upper bound for the probability of making type II errors.

For each channel \( j \in Z \) observations are described by:

\[ \forall t < \tau_j, t \in \Delta: S_j(t) = \theta_j + \sigma_j(t)\zeta_j(t) \]

\[ \forall t \geq \tau_j, t \in \Delta: S_j(t) = \theta_j + \sigma_j(t)\xi_j(t) + \theta_j(t) + \sigma_j(t)\xi_j(t). \]

where \( \{\zeta_j(t)\},\{\xi_j(t)\} \) are mutually independent random variables, \( E\zeta_j(t) = 0, E\xi_j(t) = 1, E\zeta_j(t)^2 = 1, E\xi_j(t)^2 = 1 \),

\[ \sigma_j \leq L_\sigma, \xi_j \leq L_\xi. \]

\[ \forall \theta_j \neq \theta_j, \Xi_j(t) = \theta_j(t) + \sigma_j(t)\xi_j(t) \]

is equation of target signal in \( j \)-th channel, \( \theta_j(t) > 0 \). The constants \( L_\sigma,L_\xi \) are given; noise parameters \( \{\sigma_j\} \) are unknown a priori.

The research objective is to build the signals detection procedure, which will be guarantee prescribed level for Type
I (α) and Type II (β) errors. In solving this problem for each channel we can use observations of this channel only. So, we have no possibility for use the cross-channel information, in contrast to [7]. This is due presence of huge number of channels (more than 20,000), data from which we have to process in real time.

III. SOLUTION METHOD

Let us consider the following simple statistic:

\[ \hat{\theta}_j(t, h) = \sum_{k=1}^{c-1} S_k(p) / (L_h + \delta) \cdot \frac{1}{\Delta(h) + \varepsilon^2}. \]

The \( \hat{\theta}_j(t, h) \) is non-parametric confidence upper bound for \( \theta_\tau \), and it is easy to see that \( P(\theta < \hat{\theta}_j(t, h)) \geq P \) and \( \forall \lim_{j \to \infty} \hat{\theta}_j(t, h) \to \theta \). So, interval \( (t, t + h) \) is called initial interval adaptation to noise (IIAN); calculation of \( \hat{\theta}_j(t, h) \) we will call as “adaptation to noise” (AN-procedure).

Let us consider following cycle statistics:

\[ Y_j(t \mid h, H) = (H(\Delta(h) + \varepsilon))^\frac{1}{2} \left( \sum_{k=1}^{c-1} S_k(k) \right) \]

\[ \frac{\theta_j(t, h)}{\Delta(h) + \varepsilon} + \alpha^\prime S(t) \cdot \frac{\Delta(h) + \varepsilon}{H}. \]

\[ z = \inf \{ t \geq t_i + h \mid t \geq H(L_h + L_i) \}, \]

\[ \alpha^\prime = \frac{H - (z - 1)}{L_h + L_i}, \varepsilon > 0. \]

Statistics \( Y_j(t \mid h, H) \) are defined on the sequence of the intervals:

\[ U(z, \delta_1, \delta_2, ...) = \{ u(t_i, t_i + z) \mid z \geq 1, (t_i, t_i + z, \delta_i) = (t_i, t_i + z + \delta_i, \delta_i \geq 0) \}. \]

Those cycle statistics \( Y_j(t \mid h, H) \) will be used for guarantee detection of signals by reducing the task of detection signals to the task of the moment \( \tau \) interval estimation. As confidence interval we will consider any interval \( u(t_i, z, \delta) \) from sequence \( U(z, \delta_1, \delta_2, ...) \). Once \( Y_j(u(t_i, H) \mid h) \) is calculated, we have to decide what is right: \( \tau \in u(t_i, z, \delta) \) or \( \tau \notin u(t_i, z, \delta) \). Simply put, the accuracy of moment \( \tau \) estimation is \( z \). The conditions which guarantee the prescribed quality of the algorithm are determined by the following theorem:

**Theorem 1.** Let

1. \( 1 - P \leq \alpha, 1 - P \leq \beta \).
2. \( \forall \inf_{\tau < \tau} \theta_j(t) \geq 2\Delta(h) + \varepsilon \).

3. \( H = P \left[ \left( \frac{\beta - 1 + P}{\Delta(h) + \varepsilon} \right)^2 \right] \), where

\[ b = \left( \frac{c m + 1}{c + 1} \right) c = \left( \frac{\alpha - 1 + P}{\beta - 1 + P} \right)^2, m = \frac{\Delta(h)}{\Delta(h) + \varepsilon}. \]

In this case, if the decision rule will be defined by the following way

\[ R(b) = \begin{cases} \text{if } Y_j(t \mid h, H) \geq b & \text{then } H_j \text{ is true in } j\text{-th channel} \end{cases} \]

then next inequalities will be true for prescribed \( \alpha, \beta \):

1. \( P(Y_j(t \mid h, H) < b \mid H_j : \tau \not\in u(t, z, \delta)) \leq \alpha \)
2. \( P(Y_j(t \mid h, H) > b \mid H_j : \tau \not\in u(t, z, \delta)) \leq \beta \).

**Proof of Theorem 1.** Let us consider the next representation

\[ Y_j(t - z, H) = \begin{cases} \rho_j(1) + m_j(t, H), t < \tau \end{cases} \]

\[ \rho_j(1) = \frac{\theta_j(t, h) - (1 - \alpha)}{(\Delta(h) + \varepsilon) + \alpha^\prime(1)} \]

\[ \rho_j(2) = \frac{\theta_j(t, h) - (1 - \beta)}{(\Delta(h) + \varepsilon) + \alpha^\prime(2)} \]

It is obvious that

\[ P(\rho_j(1) < \Delta(h) \frac{1}{(\Delta(h) + \varepsilon)}) \geq \beta, \]

\[ P(\rho_j(2) > 1) \geq \beta. \]

\[ m_j(t, H) = (H(\Delta(h) + \varepsilon))^\frac{1}{2} \left( \sum_{k=1}^{c-1} \frac{\sigma_j(k) \zeta_j(k)}{L_h + L_i} \right) + \sigma_j(k) \zeta_j(k) \alpha^\prime \]

\[ m_j(t, H) = (H(\Delta(h) + \varepsilon))^\frac{1}{2} \left( \sum_{k=1}^{c-1} \frac{\sigma_j(k) \zeta_j(k) + \pi_j(t) \xi_j(t)}{L_h + L_i} \right) + \sigma_j(k) \zeta_j(k) + \pi_j(t) \xi_j(t) \alpha^\prime \]

Easy to see

\[ \text{Var}(m_j(t, H) | t + z + \delta < \tau) \leq \]
On the other hand, taking into account (A.2), it easy to see

\[
P \left( Y \left( t, + z + \delta \right) | h, H \right) < b | H : \tau < u(t, z, \delta) \right) =
\]

Further, taking into account (1), we have

\[
\left( P \left( | \rho \left( 1 \right) | \geq m \right) + P \left( | \rho \left( 1 \right) | < m \right) \right) =
\]

\[
P \left( m \left( t, H \right) > b - | \rho \left( 1 \right) | - z \delta, < \tau \right) P \left( | \rho \left( 1 \right) | \geq m \right) +
\]

\[
P \left( m \left( t, H \right) > b - | \rho \left( 1 \right) | - z \delta, < \tau \right) P \left( | \rho \left( 1 \right) | < m \right) \leq P \left( | \rho \left( 1 \right) | \geq m \right) +
\]

\[
P \left( m \left( t, H \right) > b - | \rho \left( 1 \right) | - z \delta, < \tau \right) P \left( | \rho \left( 1 \right) | < m \right) =
\]

\[
P \left( \rho \left( 1 \right) \geq \Delta \left( H \right) \left( \Delta \left( h \right) + \epsilon \right)^{-1} \right) +
\]

\[
P \left( m \left( t, H \right) > b - | \rho \left( 1 \right) | - z \delta, < \tau \right) P \left( | \rho \left( 1 \right) | < m \right) \leq 1 - P_c + P \left( m \left( t, H \right) > b - | \rho \left( 1 \right) | - z \delta, < \tau \right).
\]

(3)

On the other hand, taking into account (2), it easy to see

\[
P \left( Y \left( t, + z + \delta \right) | h, H \right) < b | H : \tau < u(t, z, \delta) \right) =
\]

Here, the interval \( u(t, z, \delta) \) is simply regular interval from sequence \( U(z, \delta, \ldots) \). At usage of suggested approach, at first we calculate the cyclic statistic \( Y \left( t, + z + \delta \right) | h, H, \) for the current interval \( u(t, z, \delta) \) than we use the decision rule \( R(b) \).

We will call this method as adaptive cyclic analysis (ACA-

procedure).

IV. USAGE OF THE SUGGESTED APPROACH IN THE REAL C-OTDR MONITORING SYSTEM

The approach described in this report is used for the detection of seismoacoustic emission sources (SES) in a real C-OTDR monitoring system. The parameters of this system are: the probe pulse duration - 50 ns, frequency sensing - 3 kHz; update rate of models - 20 Hz; the probe signal power - 15 mW; laser wavelength - 1550 nm.

A. System Description

This system was installed to monitor railways (Astan area, Kazakhstan). The length of the fiber optic sensor (FOS) is 1,200 m. This sensor is buried in the vicinity of real railways (offset is 5 m, depth is 50 cm). The FOS length was divided on 1,200 logical C-OTDR channels, in the full-scale C-OTDR system there are more than 20,000 channels. Each of those channels generated the stream of primary signals (makers). Probability distributions of those signal streams are subject to the Poisson law with high intensity. That is why detection system must process signal streams very quickly. Fig. 1 shows typical distributions of the signals energy throughout the length of FOS for three frequency bands.

Fig. 2 shows typical distributions of the signal energy for another time period. We can see that these distributions are dramatically different for different time periods. Those differences are related to dynamics of influences of targeted signals and to varying influence of industrial noises. At the same time, our research has demonstrated that these differences were mostly due to influence of dynamical industrial noises.

Fig. 3 shows the targeted signal in mix with background noises. Background noise energy is bit less in comparison with targeted signal energy. In contrast to noise the targeted signal width is considerably more. This feature is very important for detection and classification of targeted signal in C-OTDR monitoring system.

Fig. 1 The distributions of the signal strength throughout the length of FOS Sample 1
Adapting to the Dynamics of the Background Noises

So, we face a situation when there are dynamical seismoacoustic industrial noises with a large stability period in the vicinity of railways. In this situation the usage of adaptive approach for signal detection proves effective. AN-procedure has been carried out during IIAN \((t_i, t_i + h)\). After that, the ACA-procedure is started. If for the \(j\)-th channel on the next interval \(u(t, z, \delta)\) it is decided that \(\tau \notin u(t, z, \delta)\), then interval \(u(t, z, \delta)\) may be used for adaptation to noise. Intervals like that we will call “interval suitable for adaptation” (ISA).

While the ACA-procedure is carried out we collect ISA-intervals until their total duration does not exceed the value \(h\). In this way we form the set of ISA-intervals. Once the total duration of ISA-intervals exceeds the value \(h\), we start the AN-procedure on the set of ISA-intervals. Thus we calculate the new value of \(\theta_j(t, h)\). After that we begin to collect a set of ISA-intervals again, repeating the whole cycle. It has proved effective.

Table I contains the results of detection of the SES. Here «Distance» is an average distance at which the given class of SEV was detected, \(P_I\) - is a detection error of type I; \(P_{II}\) - an error of type II; “Type of Noise” is the type of the background industrial noise (there are two types: “noise of water drain” (type 1), and “noise from the diesel generator” (type 2). Parameters of the detection system were as follows: \(h=200\) (since update rate of models is 20 Hz, the adaptation interval length is 10 seconds), \(\alpha = 0.2, \beta = 0.1\).

Table I shows sufficiently high practical effectiveness of the described SES detection system.

**TABLE I**

<table>
<thead>
<tr>
<th>Type of Noise</th>
<th>Distance (m)</th>
<th>(P_I)</th>
<th>(P_{II})</th>
<th>Type of noise</th>
</tr>
</thead>
<tbody>
<tr>
<td>“hand digging the soil”</td>
<td>10</td>
<td>0.15</td>
<td>0.09</td>
<td>Type 1</td>
</tr>
<tr>
<td>“chiselling ground scrap”</td>
<td>5</td>
<td>0.18</td>
<td>0.09</td>
<td>Type 2</td>
</tr>
<tr>
<td>“walking man”</td>
<td>10</td>
<td>0.19</td>
<td>0.09</td>
<td>Type 2</td>
</tr>
<tr>
<td>“cutting frozen soil”</td>
<td>15</td>
<td>0.14</td>
<td>0.1</td>
<td>Type 1</td>
</tr>
<tr>
<td>“train”</td>
<td>20</td>
<td>0.00</td>
<td>0.0</td>
<td>Type 2</td>
</tr>
</tbody>
</table>

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**REFERENCES**


