Multiple-Channel Piezoelectric Actuated Tunable Optical Filter for WDM Application

Hailu Dessalegn, T. Srinivas

Abstract—We propose new multiple-channel piezoelectric (PZT) actuated tunable optical filters based on racetrack multi-ring resonators for wavelength de-multiplexing network applications. We design tunable eight-channel wavelength de-multiplexer consisting of eight cascaded PZT actuated tunable multi-ring resonator filters with a channel spacing of 1.6nm. The filter for each channel is basically structured on a suspended beam, sandwiched with piezoelectric material and built in integrated ring resonators which are placed on the middle of the beam to gain uniform stress and linearly varying longitudinal strain. A reference single mode serially coupled multi-stage racetrack ring resonator with the same radii and coupling length is designed with a line width of 0.8974nm with a flat top pass band at 1dB of 0.5205nm and free spectral range of about 14.9nm. In each channel, a small change in the perimeter of the rings is introduced to establish the shift in resonance wavelength as per the defined channel spacing. As a result, when a DC voltage is applied, the beams will elongate, which involves mechanical deformation of the ring resonators that induces a stress and strain, which brings a change in refractive index and perimeter of the rings leading to change in the output spectrum shift providing the tunability of central wavelength in each channel. Simultaneous wave length shift as high as 45.54pm/V has been achieved with negligible tunability variation in the eight channel tunable optical filter proportional to the DC voltage applied in the structure, and it is capable of tuning up to 3.45nm in each channel with a maximum loss difference of 0.22dB in the tuning range and out of band rejection ratio of 35dB, with a low channel crosstalk ≤ 30 dB.

Keywords—Optical MEMS, piezoelectric (PZT) actuation, tunable optical filter, wavelength de-multiplexer.

I. INTRODUCTION

Optical filters are key components in wavelength-division-multiplexing networks. Such components are important to increase the bit rate for high capacity optical networks and also in switching functions for efficient signal routing. [1], it adopts a mean to bring about change in the wavelength selection, such as index alteration and light path variation. [2].

Recent active research in the microring resonators rose interests in the tunable optical filters, especially in the photonic integrated circuits [3], [4], where the high quality factor of the microring resonator is beneficial for the good filter characteristics [5]. So far, tunable wavelength filters have been reported in a number of materials utilized the index change for the wavelength tuning, such as the termoptic effect, electroptic effect, and MEMS based tuning schemes, [6]-[9].

The wavelength tuning based on the termoptic effect, however, requires local heating and demands high standing power consumption. The electroptic effect is found only in a limited number of materials. Whereas, MEMS based tuning consumes negligible standing power if a certain actuation mechanism is used, such as electrostatic and piezoelectric, those mechanisms do not require any current flow in maintaining the actuated states. In addition, it can be implemented for a much broader range of materials than those tuning methods mentioned earlier. Finally, its tuning speed can be much faster than that of the termoptic devices.

In this paper we focused on the design, simulation and analysis of a novel, multiple-channel PZT actuated tunable optical filter based on racetrack multi-ring resonators for wavelength de-multiplexing applications. Which generate a simultaneous wavelength shift of a wave propagating in the micro resonator arrays proportional to the DC voltage applied in the structure. The device model was simulated using a commercial finite element analysis tool Comsol Multiphysics and Matlab. Theoretical and simulation results are presented. The optimum design relationships are obtained.

II. EIGHT-CHANNEL PZT ACTUATED TUNABLE FILTER

The architecture of the proposed wavelength de-multiplexer is designed in a cascaded piezoelectric (PZT) actuated tunable filters as shown in Fig. 1. The design of each filter involves the design of piezoelectric actuated beam, optical integrated ring resonator and opto-mechanical coupling between them. It is basically structured on a sandwiched beam, piezoelectric material (PZT-5A) sandwiched between two SiO₂ layers and built in optical integrated ring resonator which is placed on the middle of each beam to gain uniform stress, linearly varying displacement on the longitudinal direction and ideally, zero displacement on the other directions.

When a DC voltage is applied longitudinally, the beams will elongate, which involves mechanical deformation in the ring resonator arrays that induces a stress and strain, which brings a change in refractive index and perimeter of the rings leading to change in the output spectrum shift providing the tunability of central wavelength in each channel.

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The intensity transfer function for a three-ring resonator is
\[ T = t_0, t_1, t_2, t_3, e^{\delta_{13}+\delta_{12}+\delta_{32}}. \]  
where, \( t_j = \sqrt{(1-K_j)(1-r_j)} \) effective transmission coefficient of the coupler, \( r_j = \sqrt{K_j(1-r_j)} \) effective reflection coefficient of the coupler, \( K_j \) is the coupling coefficient for \( j=0, 1, 2 \) and \( 3 \) respectively, and \( \beta \) and \( \alpha \) is the propagation constant and attenuation constant of a waveguide respectively.

B. Eight-Channel Dropping Filter

Here, it employed a simplest method to achieve multiple-channel filters consisting of serially coupled racetrack ring resonator arrays in silicon, where the individual resonance wavelength of each racetrack multi-ring resonator in the array is shifted by changing its perimeter [4].

Race-track shaped multi-ring resonators were chosen for analysis, and design. The reference resonator’s perimeter is \( P=2\pi(L_c+\pi R) \). The perimeter is varied by adjusting the radius of the curved portions of the racetrack multi-ring resonator from \( R \) to \( R+\Delta R \), i.e., \( \Delta P=2\pi \Delta R \), while the coupling lengths \( (L_{c0}) \) are kept constant.

As the silicon waveguide has very large dispersion, the effective index varies when the resonance wavelength changes. Then, the resonance condition for the two resonators shown with a dotted line in Fig. 1 is

\[ m\lambda_0 = 2\pi R n_b + 2L_{c0} n_b \]  
\[ m(\lambda_0 + \Delta\lambda) = 2\pi (R + \Delta R)(n_b + \Delta n_b) + 2L_{c0} (n_s + \Delta n_s) \]  

where \( m \) is an integer (resonance order), \( \lambda_0 \) is the reference resonating wavelength, \( n_b \) is the effective index in the straight waveguide, and \( n_s \) is the effective index in the bending waveguide.

As it is outlined in paper [4], the resonance frequency shift \( \Delta\lambda \) can be approximated as:

\[ \Delta\lambda = \left( \frac{\Delta P}{P} \right) \left( T - 1 \right) \left( 1 - \frac{\lambda_0}{n_s} \times \frac{\lambda_0(n_b+n_s)}{\lambda_0+n_s} \right) \]
Fig. 2 Output characteristics of eight-channel serially coupled multi-stage racetrack ring resonator arrays with no load

Fig. 2 shows the output intensities as a function of wave length at the drop port and it has been achieved a line width of 0.8974nm in the reference ring resonator with a flat top pass band at 1dB of 0.5205nm and free spectral range of about 14.9nm. Also, it has been observed a line width incremental of 0.0009nm for the successive channel which results a change in the flat top pass band at 1dB of 0.0005nm in each successive channel.

C. Piezoelectric Actuated Beam

The geometry in Fig. 1 was analyzed using numerical simulations with Comsol Multiphysics finite element modelling software. Each beam comprised optimal design demission of a 30µm(l) x 300µm(w) x 2µm(h) a sandwiched silicon dioxide (SiO₂) cantilever beam, with a buried piezoelectric material of 1.6µm thickness(H) to get negligible displacement in the middle of the beam in both the y and z components as shown in Fig. 3 where, l, w and h represent the length, width and thickness of the beam, respectively.

The DC voltage applied to the electrodes causes each beam to develop stress and strain. Thus, for thin silicon, ignoring the sheer stress and normal stress effect on optical performance, the longitudinal stress ($T_l$) and transversal stress ($T_t$) in the middle of each beam can be defined as:

$$T_l = E \cdot d_{33} \cdot \left(\frac{y}{h}\right) \cdot \left(\frac{h}{w}\right)$$

$$T_t = E \cdot d_{31} \cdot \left(\frac{y}{h}\right) \cdot \left(\frac{h}{w}\right)$$

where, $E$ is young's modulus, $d_{33}$ and $d_{31}$ is longitudinal and transverse piezoelectric coefficients of the material, respectively.

![Fig. 4 Stress tensor in the X, Y or Z component versus (a) Width of the beam (b) Length of the beam](image-url)
edges. Hence, the resonators’ waveguides is located there to gain uniform refractive index change in each waveguide.

Similarly, strain can be defined as

$$\Delta \epsilon = \left( \frac{T_1 - v T_1}{E} \right)$$  \hspace{1cm} (10)

$$\Delta \epsilon = \left( \frac{T_2 - v T_1}{E} \right)$$  \hspace{1cm} (11)

This tells us that, as the applied voltage increases the longitudinal strain increase. Which intern affects the coupling length and the shape of the rings whereas, the transverse strain is almost zero in the middle, as it is shown in Fig. 5, which has insignificant effect on the inter waveguide gap and the shape of the rings where, $\nu$ is Poisson’s ratio.

\[ \Delta \varphi = \frac{2 \pi}{A} \Delta n_{eff} \left( 2 \pi R \right) + n_{eff} \Delta \tilde{P} \]  \hspace{1cm} (14)

\[ \Delta P_{eff} = 2 \left( L_c - L_{\text{eff}} \right) + \left( P_{\text{ellipse}} - 2 \pi R \right) \]  \hspace{1cm} (15)

where $\Delta P_{eff}$ is change in the total circumference of the ring due to applied voltage and $P_{\text{ellipse}}$ is the circumference of the curves in both sides of the couplers.

III. RESULT

Thus, the resonance wavelength shift $\Delta \lambda_r$ as a function of effective refractive index change and the total circumference change of the ring $\Delta P_{eff}$ can be written as

$$\Delta \lambda_r = \frac{2 \Delta n_{eff} \left( 2 \pi R + 2L_{\text{eff}} \right) + n_{eff} \Delta P_{eff}}{m}$$  \hspace{1cm} (16)

where, m is the mode number and it is to be m=52.

To investigate tunability of a multi-channel filter in our design, we actuated each beam. When controlling the actuation voltage of each beam simultaneously, input range from (0 to 60) V, Fig. 6 shows the transmission spectra versus input wavelength variation for an applied voltage of different values at the drop port of each channel. The curve shows the tunability of the optical filter with in the incremental of 5V of applied voltage. It is observed from the graph that there is a change in the typical parameters as it is shown in Table I. The bandwidth variation with an incremental of 0.0009nm from its’ adjacent channel has been observed due to the change in perimeter and strain effect on the rings. It results a tenability variation of 0.05pm in each channel. A simultaneous linear variation of the wavelength shift as high as 45.54 pm/V has been achieved with a negligible tunability variation in the eight channel tunable optical filter proportional to the DC voltage applied in the structure, and it is capable of tuning up to 3.45 nm in each channel with a maximum loss difference of 0.22dB in the tuning range.
### TABLE I

**TYPICAL CHANNEL PARAMETERS FOR THE EIGHT CHANNELS TUNABLE OPTICAL FILTER**

<table>
<thead>
<tr>
<th>Channel</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
</tr>
</thead>
<tbody>
<tr>
<td>Center wavelength (nm)</td>
<td>1547.3028</td>
<td>1548.9008</td>
<td>1550.4989</td>
<td>1552.0969</td>
<td>1553.6949</td>
<td>1555.2930</td>
<td>1556.8910</td>
<td>1557.1194</td>
</tr>
<tr>
<td>1dB bandwidth (nm)</td>
<td>0.5205</td>
<td>0.5210</td>
<td>0.5215</td>
<td>0.5220</td>
<td>0.5225</td>
<td>0.5230</td>
<td>0.5235</td>
<td>0.5240</td>
</tr>
<tr>
<td>3dB bandwidth (nm)</td>
<td>0.8974</td>
<td>0.8983</td>
<td>0.8992</td>
<td>0.9001</td>
<td>0.9010</td>
<td>0.9019</td>
<td>0.9028</td>
<td>0.9037</td>
</tr>
<tr>
<td>Tunability (pm/V)</td>
<td>45.42</td>
<td>45.46</td>
<td>45.50</td>
<td>45.54</td>
<td>45.58</td>
<td>45.62</td>
<td>45.66</td>
<td>45.70</td>
</tr>
<tr>
<td>Spacing (nm)</td>
<td>1.598</td>
<td></td>
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<td>Loss difference (dB)</td>
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<td></td>
<td></td>
<td></td>
<td></td>
<td>0.2218</td>
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<tr>
<td>Band rejection ratio (dB)</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>35</td>
<td></td>
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<tr>
<td>Channel crosstalk (dB)</td>
<td></td>
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<td></td>
<td></td>
<td></td>
<td></td>
<td>&lt; 30</td>
<td></td>
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<tr>
<td>Tuning Range (nm)</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>3.45</td>
<td></td>
</tr>
</tbody>
</table>

### IV. CONCLUSION

We have proposed and analysed novel eight-channel piezoelectric (PZT) actuated tunable optical filter based on racetrack multi-ring resonators for the first time for wavelength de-multiplexing applications. We design tunable eight-channel wavelength de-multiplexer consists of eight cascaded PZT actuated tunable multi-ring resonator filters with a channel spacing of 1.6nm. A small change in the perimeters of the rings is introduced to establish the shift in resonance wavelength according to the defined channel spacing and it has been achieved a negligible tunability variation with a flat top pass band incremental at 1dB of 0.0005nm. Also, the effects of the coupling coefficients on each resonance are investigated. Moreover, the piezoelectric actuated beam is optimally designed to maximize the uniform stress on the middle of the beam and linearly varying strain along the length while reducing strain in the other direction.

The wavelength shift as high as 45.54pm/\(V\) has been achieved in eight channel tunable optical filter proportional to the DC voltage applied in the structure, and it is capable of tuning up to 3.45nm in each channel with a maximum loss difference of 0.22dB in the tuning range and out of band rejection ratio of 35dB, with a low channel crosstalk ≤ 30 dB.

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### REFERENCES


