Optimization Parameters of Rotary Positioner Controller using CDM

Meemongkol A., Tipsuwanporn V. and Numsomran A.

Abstract—The authors present optimization parameters of rotary positioner controller in hard disk drive servo track writing process using coefficient diagram method; CDM. Due to estimation parameters in PI Positioning Control System by expected ratio method cannot meet the required specification of response effectively, we suggest coefficient diagram method for defining controller parameters under the requirement of the system. Finally, the simulation results show that our proposed method can improve the problem in tuning parameter of rotary positioner controller. It is satisfied specification of performance of control system. Furthermore, it is very convenient as a fast adjustment damping ratio as well as a high speed response.

Keywords—Optimization Parameters, Rotary Positioner, CDM

I. INTRODUCTION

Rotary positioner control system in No Clock Head servo track writer control the product actuator during the servo write process by PI controller which is configured to suit various specifications by setting controller parameters.

Problem that occurred with the parameters adjustment in PI Positioning Control System of Rotary Positoner is estimating them from the related ratio that recommended by user manual [1] cannot meet the desired specification response. Due to the relation of parameters in control system, tuning them formlessly cannot meet the required specification of response and causes time wasting. This paper proposes optimization the parameters of PI Rotary Positioner Control System using Coefficient Diagram Method which is satisfied specification of performance of control system. Furthermore, it is very convenient as a fast adjustment damping ratio as well as a high speed response.

The details of our proposed method and experiment are described clearly as the following topic. In section 2 has the detail of Position control of rotary Positioner in servo track writing process. In section 3 explains the detail of Coefficient Diagram Method. In section 4 describes the detail of Numerical Experiment. In section 5 has the detail of Simulation & Results and the conclusion is explained in section 6.

II. POSITION CONTROL OF ROTARY POSITIONER IN SERVO TRACK WRITING PROCESS

A. Rotary Positioner Control System

Rotary Positioner Control System is one of the most important parts of conventional servo track writer. It is used to control the product actuator during the servo write process. In Figure 1 shows structure of one cell servo track writer experimental equipment that consists of the first part as personal computer (PC). It executes test code for monitor and controls all procedures in servo track writing process. The second part is block of control/driver and interface card which consist of radial card, R/W motor card, clock pattern card and DE IF card.

The third significant part is the part of positioning control in rotary positioner control system which plays a crucial role as it carries out the positioning of R/W head. It consists of rotary positioner (Motor/Encoder KP-1M) and positioner control card (System Controller : SC-01H/PC) which receives commands and the value of positioning control parameters from PC in the form of execute software. Then the positioning control are controlled by an on-board DSP, which runs its own task to generate the suitable control signal and send the signal to drive circuit and rotary positioner respectively.

B. Parameters of Rotary Positioner Control System

This section describes the parameters which are used in this rotary positioner system. The rotary positioner system can be...
configured to suit various specifications by setting parameters. The parameters are sent to the rotary positioner from the host computer via the interface.

This parameter fixes cut off frequency of low pass filter. A typical value for this parameter is four times as large as the speed loop gain. The lower the cut-off frequency $W_f$ is, the smaller the noise in the system becomes. Setting $W_f$ too low, however, affects the system stability and requires longer setting time.

C. Problems with parameter tuning of Rotary Positioner Controller

Problem that occurred with the parameters adjustment in PI Positioning Control System of Rotary Positioner is estimating them from the related ratio that recommended by user manual cannot meet the desired position response.

Due to the relation of parameters in control system, tuning them formlessly cannot meet the required specification of response and causes time wasting.

This paper proposes optimization the parameters of PI Rotary Positioner Control System using Coefficient Diagram Method which is satisfied specification of performance of control system. Furthermore, it is very convenient as a fast adjustment damping ratio as well as a high speed response.

III. COEFFICIENT DIAGRAM METHOD

The CDM [2, 3] is used for design the controller so that the step response of the controlled system satisfies both transient and steady state response specifications, and also satisfies the requirements of stability, faster response and robustness.

Coefficient Diagram is used for investigating the stability, time response and robustness characteristics of systems in a single diagram, which is important for systems with large characteristic polynomial degree.

The block diagram of CDM design for a single input-single output (SISO) system is shown in Fig 4. Here $Y(s)$ is the output signal, $R(s)$ is the reference input, $D(s)$ is the disturbance. $B_p(s)$ and $A_p(s)$ are numerator and denominator of transfer function of the plant, respectively. $B_c(s)$ and $A_c(s)$ are numerator and denominator of transfer function of the controller.

The polynomials form of the controller and the plant are generally be written respectively in the form [4].

$$A_c(s) = l_1 s^2 + l_2 s + l_0$$

$$B_c(s) = k_1 s^2 + k_2 s + k_0$$

and

$$A_p(s) = P_k s^k + P_{k-1} s^{k-1} + \ldots + P_0$$
\[ B_p(s) = q_m s^m + q_m-1 s^{m-1} + \ldots + q_0 \]  
where \( \lambda < k \) and \( m < k \)

When we neglect the effect by disturbance \( D(s) \), closed loop transfer function become \( G_c(s) \) in eq. (5).

\[ G_c(s) = \frac{Y(s)}{R(s)} = \frac{B_p(s)}{A_c(s)A_p(s) + B_c(s)B_p(s)} \]  
the characteristic polynomial and given by

\[ P(s) = a_n s^n + a_{n-1} s^{n-1} + \ldots + a_1 s + a_0 \]  
where \( a_0, a_1, \ldots, a_n \) are the real coefficients. The stability index \( \gamma_i \) the equivalent time constant \( \tau \) and the stability limit \( \gamma_i^* \) are defined as follows:

\[ \gamma_i = \frac{a_i}{a_i \gamma_{i-1} + 1}, \quad i = 1, \ldots, n - 1, \quad \gamma_0 = \gamma_n = \infty \]  
\[ \tau = \frac{a_0}{a_0} \]  
\[ \gamma_i^* = \frac{1}{\gamma_{i-1} + 1} \]  
(9)

From Eq. (6) - (8), the coefficients \( a_i \) and the characteristic equation \( P(s) \) are

\[ a_i = a_0 \left( \frac{1}{\gamma_{i-1} \cdots \gamma_{i-j} \gamma_i^*} \right)^{j-1} \]  
\[ P(s) = a_0 \left( \sum_{j=2}^{n} \prod_{j=2}^{i} \left( \gamma_j^* \right) \right) + a_1 s + a_0 \]  
(11)

The coefficients in Eq. (5) came from the chosen stability index \( \gamma_i \) and equivalent time constant \( \tau \) by equating the \( P(s) \) of Eq. (5) with the characteristic equation of Rotary Positioner control system, such that the parameters of PI controller are obtained.

### IV. CONTROLLER DESIGN FOR THE ROTARY POSITIONER SYSTEM

In this section, the design procedures of PI Controller via CDM where PI Controller transfer function is Eq. (12)

\[ G_c(s) = \frac{W_c s + W_o W_a}{s} \]  
(12)

Rotary Positioner closed loop system transfer function is expressed as below.

\[ G_c(s) = \frac{W_c s + W_o W_a}{T_f s + 1 + W_c s + W_o W_a} \]  
(13)

The equivalent time constant \( \tau \) is chosen as \( \tau = t_f / 2.58 \) where \( t_f \) is the specified settling time.

Stability indices for Rotary Positioner system came from the best value that gave best simulation results. It is different from standard form [4] but still achieve the desired characteristics for the controller

Stability index \( \gamma_1 = 4, \gamma_2 = 1.4286, \gamma_3 = 5 \)

The stability limits are computed from Eq.9 to be

\[ \gamma_i^* = [0.699, 0.45, 0.699] \]  
i = 1 ~ 3, \( \gamma_0, \gamma_4 = \infty \)

the \( P(s) \) can be expressed as

\[ P(s) = a_6 s^6 + a_5 s^5 + a_4 s^4 + a_3 s^3 + a_2 s^2 + a_1 s + a_0 \]  
(14)

and characteristic equation of closed loop transfer function is

\[ P_c(s) = T_f s + 1 + W_c s + W_o W_a \]  
(15)

Equated the above \( P(s) \) to the \( P_c(s) \) of the plant in Eq. (15), the parameters of PI controller are obtained as Eq. (16)-(17).

\[ W_c = \frac{1}{\gamma_1 \gamma_2 \gamma_3 \gamma_4} \]  
(16)

\[ W_o = \frac{\gamma_1 - W_o \tau}{\tau} \]  
(17)

### V. SIMULATION & RESULTS

In this paper, the simulation results of rotary positioner positioning control is given by MATLAB Simulink program. The simulation in Fig. 4 illustrates optimization of PI controller’s parameters using Coefficient Diagram Method which is satisfied specification of performance of control system and explain about adjustment of response speed and its overshoot by CDM technique.

![Fig. 4 Simulation System](Image)

Plant Parameters was shown in Table I.

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>( T_f )</td>
<td>1/Cut off frequency</td>
<td>0.0001 [sec/rad]</td>
</tr>
<tr>
<td>( W_c )</td>
<td>Position Loop Gain</td>
<td>700 [rad/sec]</td>
</tr>
<tr>
<td>( W_o )</td>
<td>Speed Loop Gain</td>
<td>( (\gamma_1 - W_o \tau) / \tau )</td>
</tr>
<tr>
<td>( W_a )</td>
<td>Integration Constant</td>
<td>( \gamma_1 \cdot \gamma_2 / \tau )</td>
</tr>
</tbody>
</table>

From this data formed by Eq. (15) then it is obtained the characteristic equation of closed loop transfer function as

\[ P_c(s) = (1e-3 s^4 + 3 s^3 + 7 s^2 + 10 s + 700 + W_o) \]  
(18)

According to Eq. (14), design of PI controller based on CDM, is assigned parameter follow as time constant \( \tau = 0.0029 \). The stability index \( \gamma_1 = 4, \gamma_2 = 1.4286, \gamma_3 = 5 \) then the characteristic equation is,

\[ P(s) = (1e-3 s^4 + (9.99e-1) s^3 + (1.97e+3) s^2 + (2.71e+6) s + 9.36e+8) \]  
(19)
Equated the above $P_D(s)$ in Eq. (18) to the $P(s)$ of the plant with the PI controller in Eq. (19), the parameters of PI controller are

\[ W_c = 1970.50 \quad W_a = 679.31 \]

The step response in Fig.5, showed the response’s overshoot which is over 0 percent and settling time is at 0.0065 msec.

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Adjustment speed response by using CDM method for optimization of PI controller’s parameters are described as follow details.

The characteristic equation is,

\[ P(s) = (1e-3)s^4 + (9.99e-1)k_3s^3 + (1.97e+3)k_4s^2 + (2.71e+6)k_5s + (9.36e+8)k_6 \]

where $k$ are 0.7, 1, 3 respectively.

Assign parameter follow as time constant $\tau=0.0029$, The stability index $\gamma_1 = 4, \gamma_2 = 1.4286, \gamma_3 = 5$.

Equated the above $P_D(s)$ in Eq. (18) to the $P(s)$ of the plant with the PI controller in Eq. (20), and the parameter of PI controller are given as shown in table II.

Fig 7 shows that, when $k$ is adjusted, setting time is decreased from 0.0085 sec. to 0.0065 sec. to 0.0057 sec. therefore; the system response is faster.

TABLE II

<table>
<thead>
<tr>
<th>$k$</th>
<th>$W_c$</th>
<th>$W_a$</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.7</td>
<td>1379.30</td>
<td>265.51</td>
</tr>
<tr>
<td>1</td>
<td>1970.50</td>
<td>679.31</td>
</tr>
<tr>
<td>3</td>
<td>5911.40</td>
<td>3437.90</td>
</tr>
</tbody>
</table>

Adjustment overshoot of response by using CDM method for optimization of PI controller’s parameters are described as follow details.

The characteristic equation is,

\[ P(s) = (1e-3)s^4 + (9.99e-1)k_3s^3 + (1.97e+3)k_4s^2 + (2.71e+6)k_5s + (9.36e+8)k_6 \]

where $k$ are 0.85, 1, 1.5 respectively.

Equated the above $P_D(s)$ in Eq. (18) to the $P(s)$ of the plant with the PI controller in Eq. (21), then the parameter of PI controller are given as shown in table III.
TABLE III
Controller Parameters

<table>
<thead>
<tr>
<th>$k$</th>
<th>$W_c$</th>
<th>$W_a$</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.85</td>
<td>1423.70</td>
<td>472.41</td>
</tr>
<tr>
<td>1</td>
<td>1970.50</td>
<td>679.31</td>
</tr>
<tr>
<td>1.5</td>
<td>4433.60</td>
<td>1369.00</td>
</tr>
</tbody>
</table>

Fig. 9. Overshoot Adjustment of Step Response of Rotary Positioner Control System

Fig. 10. Control Signal of Controller

Fig 9 shows the step response, when $k$ is changed 0.85 to 1 and 1.5 respectively then the damping ratio is also increased but the overshoot is decreased from 3.24 percent to 0%.

As shown simulation results, we can conclude that Coefficient Diagram Method can be used for optimization the parameters of PI Rotary Positioner Control System and satisfy specification of performance of control system. Furthermore, it is very convenient as a fast adjustment damping ratio as well as a high speed response.

VI. CONCLUSION

In this paper, optimization the parameters of PI Rotary Positioner Control System using Coefficient Diagram Method is presented. The simulation results from MATLAB are able to illustrate that CDM Techniques can be applied to Positioning Control System of Rotary Positioner for solving the problem in tuning controller parameters. Its advantage which only one parameter is to be adjusted, speed and overshoot response is changed and satisfied the required response specification.

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REFERENCES