Abstract—This paper presents a comparison between two Pulse Width Modulation (PWM) algorithms applied to a three-level Neutral Point Clamped (NPC) Voltage Source Inverter (VSI). The first algorithm applied is the triangular-sinusoidal strategy; the second is the Space Vector Pulse Width Modulation (SVPWM) strategy. In the first part, we present a topology of three-level NPC VSI. After that, we develop the two PWM strategies to control this converter. At the end the experimental results are presented.

Keywords—Multilevel inverter, Space vector pulse width modulation (SVPWM), triangular-sinusoidal strategy.

I. INTRODUCTION

RECENTLY, developments in power electronics and semiconductor technology have lead improvements in lower electronic systems. Hence, different circuit configurations namely multilevel inverters have become popular and considerable interest by researcher are given on them [1-2]. Three-level Neutral Point Clamped (NPC) inverter shown in Fig. 1 has evolved into the standard for medium voltage motor drive systems as evidenced by the commercial availability of medium voltage drives based on both IGCT and high voltage IGBT devices. The topology has two important attributes that make it well suited to this market: lower harmonic content than a standard two level inverter, and the fact that the main switching devices are required to block only one-half of the dc bus voltage. This latter attribute has traditionally been exploited to allow for higher voltage drives since device voltages have been limited. However, it also implies that a drive of a given voltage can be obtained with lower voltage devices by employing the NPC topology.

Various PWM techniques for the three-level converter have been intensively studied since Nabae proposed the topology named neutral point clamped converter [3]. In various PWM techniques, the three-level SVPWM is one of most promising and widely applied PWM techniques in three phase systems. It is a naturally accepted view that three-level SVPWM is an extension of the conventional two-level SVPWM.

II. MODELLING OF THREE-LEVEL NPC VOLTAGE SOURCE INVETER

The three phases three-level NPC VSI is constituted by

K. Benamrane, T. Abdelkrim, Aeh. Benkhelifa, and B. Bezza are with Division of Small Solar Plants, Unit of Applied Research in Renewable Energies, EPSTL Center for Renewable Energy Development, PBox 88 Gart Taam, 47133 Ghardaïa, Algeria (e-mail: Kbenamrane7@gmail.com).

T. Benslimane is with the Laboratory of Automation and Electrification of Industrial Enterprises, University of Boumerdes; University of M’sila BP. 166, street Ichbilia, M’sila, Algeria (e-mail: bens082002@yahoo.fr).

As indicated in Table I, each leg of the inverter can have three possible switching states, P, O, or N. When the top two switches T11 and T12 are turned on, the switching state is P. When the medium switches T12 and T13 are turned on, switching state is O. When the lower switches T13 and T14 are turned on, the switching state is N.

Fig. 2 shows the space vector diagram for three-level inverter. Since three kinds of switching states exist in each leg,
this converter has 27 switching states, as indicated in the diagram. The output voltage vector can take only 18 discrete positions in the diagram because some switches state are redundant and create the same space vector.

TABLE I

<table>
<thead>
<tr>
<th>Switching Symbols</th>
<th>Switching States</th>
<th>Output Voltage</th>
</tr>
</thead>
<tbody>
<tr>
<td>T1, T2, T3, T4</td>
<td>P ON ON OFF OFF</td>
<td>U1a</td>
</tr>
<tr>
<td></td>
<td>O ON OFF ON ON</td>
<td>0</td>
</tr>
<tr>
<td></td>
<td>N OFF OFF ON ON</td>
<td>-U2a</td>
</tr>
</tbody>
</table>

![Fig. 2 Space vector diagram of a three-level inverter]

III. THREE-LEVEL INVERTER CONTROL

A. Algorithm 1

This algorithm is based on the triangular-sinusoidal strategy with two carriers [5-6], is divided to four parts.

1. Part 1
   Determination of the generating conversion functions $n_{gK}$:
   \[ n_{gK} = \frac{V_{ref}}{E/2} \] (4)

2. Part 2
   Determination of the half leg generating connection functions $F^b_{Kmg}$:
   \[ F^b_{K1g} = \frac{n_{k1}}{2}, \quad F^b_{K0g} = \frac{n_{k0}}{2} \] (5)

3. Part 3
   Determination of the half leg connection functions $F^b_{Km}$

\[ \begin{cases} T_{k1} = T_c (1 - |F^b_{K1}|) \\ T_{k0} = T_c (\frac{1}{2} - |F^b_{K0}|) \end{cases} \] (6)

\[ \begin{cases} \frac{T_c}{2} < \frac{T_{k1}}{2} \Rightarrow \alpha_c = 1 \\ (\frac{T_{k1}}{2} < \frac{T_{k0}}{2} \text{ and } \frac{T_{k0}}{2} < \frac{T_c}{2}) \Rightarrow \alpha_c = 0 \end{cases} \] (7)

\[ \begin{cases} F^b_{K1} > 0 \Rightarrow (F^b_{K1} = a_k) \text{ and } (F^b_{K0} = 0) \\ F^b_{K0} \leq 0 \Rightarrow (F^b_{K1} = 0) \text{ and } (F^b_{K0} = a_k) \end{cases} \] (8)

4. Part 4
   Determination of the control order of the switch $B_{ki}$

\[ \begin{cases} ((F^b_{K1} = 1) \text{ and } (F^b_{K0} = 1)) \\ \text{or} \\ ((F^b_{K1} = 0) \text{ and } (F^b_{K0} = 0)) \end{cases} \Rightarrow F_{K1} = 1, F_{K2} = 0 \] (9)

\[ \begin{cases} ((F^b_{K1} = 1) \text{ and } (F^b_{K0} = 0)) \\ \text{or} \\ ((F^b_{K1} = 0) \text{ and } (F^b_{K0} = 1)) \end{cases} \Rightarrow F_{K1} = 1, F_{K2} = 1 \] (10)

The Fig. 3 shows the simple output voltage of the three-level NPC VSI controlled by the proposed algebraic strategy for $m=12$ and $r=0.8$. The spectral analysis of this voltage shows that the total harmonics distortion is higher than 60%.

![Fig. 3 Simple output voltage $V_A$ and its spectral analysis for $m=12$, $r=0.8$]

B. Algorithm 2

27 vectors can construct the space-vector diagram of a three level converter, shown as Fig. 2. There are 24 active vectors including 12 short vectors, 6 medium vectors and 6 long vectors, and the remaining three are zero vectors (PPP, OOO, NNN), which lie at the center of the hexagon [7-8]. The area of the hexagon can be divided into six sectors (A to F), each of which has four regions (1 to 4), with 24 regions of operation in...
total. This algorithm used in this paper is composed by six steps described in the following Fig. 4.

**Step 1**
Calculation of the reference vector $V_{ref}$

**Step 2**
Calculation of phase angle $\theta$ and sector $i$

**Step 3**
Translation to the first sector

**Step 4**
Determination of region (1 to 4)

**Step 5**
Determining of vectors and calculating the periods of switching

**Step 6**
Return to the initial sector

Fig. 4 Steps of SVPWM

The Fig. 5 shows the simple output voltage of the three-level NPC VSI controlled by the proposed Space Vector Pulse Width Modulation strategy for $m=12$ and $r=0.8$. The spectral analysis of this voltage shows that the total harmonics distortion is lower than 40.

![Fig. 5 Simple output voltage $V_a$ and its spectral analysis for $m=24$, $r=0.8$](image)

**IV. EXPERIMENTAL RESULT**

The input voltage of the three-level neutral point clamped voltage source inverter is $E = 60V$. This converter fed a three phases R-L load where $R=22\Omega$ and $L=340mH$.

Figs. 6 and 9 present the voltage $V_{AM}$ of the first leg of inverter controlled by algorithms 1 and 2. The output voltage $V_A$ and its spectral analysis for the two algorithms are presented in Figs. 7, 8, 10 and 11.

One remarks that the total harmonics distortion obtained by the second algorithm is better than the THD obtained by the first algorithm.
CONCLUSION

This paper presents the comparison between two algorithms of the three-level NPC converter. The modelling of this inverter shows that it is equivalent to two two-level inverters in series.

The triangular-sinusoidal and space vector PWM algorithms for a three level inverter have been simulated using C++. Simulation and experimental results have been given for R-L load. It has been shown that high quality of waveforms obtained by space vector PWM strategy.

REFERENCES


