The Biomechanical Properties of the Different Modalities of Surgically Corrected Coarctation of the Aorta in Neonates and Infants

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Abstract—Biomechanical properties of infantile aorta in vitro in cases of different standard anastomoses: end-to-end (ETE), extended anastomosis end-to-end (EEET) and subclavian flap aortoplasty (SFA) used for surgical correction of coarctation were analyzed to determine the influence of the method on the biomechanics of infantile aorta and possible changes in haemodynamics. 10 specimens of native aorta, 3 specimens with ETE, 4 EEET and 3 SFA were investigated. The experiments showed a non-linear relationship between stress and strain in the infantile aorta, the modulus of elasticity of the aortic wall increased with the increase of inner pressure. In the case of anastomosis end-to-end the modulus was almost constant, relevant to the modulus of elasticity of the aorta with the inner pressure 100-120 mmHg. The anastomoses EETE and SFA showed elastic properties closer to native aorta, the stiffness of ETE did not change with the changes in inner pressure.

Keywords—biomechanics, coarctation, mechanical properties, neonatal aorta

I. INTRODUCTION

The incidence of congenital heart diseases (CHD) is 8-12 per 1000 live born infants and approximately one quarter of these children are affected by critical CHD which requires surgical or catheter intervention within the first year of life [1]. Aortic coarctation (narrowing of the descending aorta usually just distal to the origin of the left subclavian artery) accounts for 6-10% of CHD with the prevalence approximately 36 (29-49)/100 000 newborn infants [2], [3]. The data from literature confirm surgical treatment to be the gold standard for the treatment of the coarctation in neonates and small infants due to less complications and lower incidence of recoarctation in comparison to balloon angioplasty in this particular age group. The method of choice for the surgical treatment varies between different centers and surgeons with extended anastomosis end-to-end (EEET) most often preferred [7]-[11]. Subclavian flap aortoplasty is also used [12]-[14] in the cases of infantile coarctation with isthmus hypoplasia and/or hypoplasia of the transverse arch, but anastomosis end-to-end performed in isolated coarctations in older infants[15], [16]. Such complications as recoarctation and secondary arterial hypertension frequently occur even after successful surgical repair probably related to the loss of the arterial elasticity. There are still discussions according the choice of treatment [17].

II. AIM OF THE STUDY

To investigate the biomechanical properties of the aorta in neonates and infants and to compare the biomechanical properties of the aorta in case of different techniques of anastomoses.

III. MATERIALS AND METHODS

The study was approved by ethics committee of The University Hospital for Children.

A. Material preparation

During the period of time from April 2009 till December 2011, 20 specimens (40 mm in length) of the upper part of the descending aorta during autopsies of neonates and infants (patients without the diagnosis of coarctation) were acquired. The age of the patients was 1 day to 5 months (mean age 31.94 ± 49.29 days, mean weight 3.86 ± 1.25 kg, minimum weight 2 kg and maximum weight 6.7 kg). The vessels were marked before resetting to identify the in situ axial length. The anastomoses were made by the cardiac surgeon performing the kind of operations in the clinic using suture techniques identical to operation in vivo with uninterrupted sutures with Prolen 6.0-7.0 in the posterior and several interrupted sutures on the front wall. The specimens were preserved in Custodiol® Perfusion Solution (Custodiol® HTK Solution for perfusion and flushing donor organs) not longer than 24 hours at temperature 2-4°C.

B. Experimental Procedure

A special experimental set up with video camera connected to the laptop was used to measure the internal pressure, axial force, longitudinal and circumferential deformation of the aorta as in Fig. 1.
An aortic sample was gradually loaded by internal pressure from 0 to 220 mmHg while maintaining the length of the sample constant at \( L_0 \), the length \textit{in situ}. The pressure was elevated in 20 mmHg steps with pressure held constant in each step for 1 minute. The initial external diameter at inner pressure \( p = 0 \) mmHg and at \textit{in situ} axial length \( L_0 \) was noted as \( D_0 \). The diameter \( D \) was recorded at each pressure level. The value of the wall thickness \( h \) was calculated as follows:

\[
\begin{align*}
\lambda_3 &= \frac{1}{\lambda_1 \lambda_2}, \\
\lambda_2 &= \frac{D}{D_0},
\end{align*}
\]

The circumferential stress was calculated as:

\[
\sigma = \frac{pR}{h},
\]

where \( p \) - inner pressure, \( R \) - radius.

\[
\lambda_1 = \frac{L}{L_0} = 1.0.
\]

In these equations, \( h_0 \) is the initial thickness of the specimen wall and \( \lambda_1, \lambda_2 \) and \( \lambda_3 \) are, respectively, the stretch ratios in the axial, circumferential, and radial directions. Because the length of the artery was maintained constant at \( L_0 \), the value of \( \lambda_1(= L/L_0) \) was one. The initial wall thickness \( h_0 \) was measured with a catheterometer with \( \pm 0.001 \) mm accuracy. The artery was preconditioned before tests by subjecting it to cyclic loading to bring it to a stable state to give more reproducible mechanical response. During this process, the vessel was pressurized from 0 to 220 mmHg in 20 steps five times with pressure held constant for 1 minute at each step. The initial curves were markedly hysteretic, but the third or fourth cycle gave reproducible curves with minimal hysteresis. A modulus of elasticity \( E \) was calculated as incremental modulus between two values of internal pressure as in Fig.2.

The histological examination (light microscopy) of the aortic wall was performed before and following the experiments.

### RESULTS

Our data show non-linear relationship between stress and strain in neonatal and infantile aorta. The wall thickness of the samples was 1.1±0.0934 mm (minimum 0.91 mm, maximum 1.26 mm, median 1.125 mm, mode 1.06 mm). The strain of the aorta at inner pressure 60 was 25.12 ± 9.37 %, at 80 mmHg was 29.3 ± 11.62 %, but at 100 mmHg was 32.62 ± 13.37 % (Table I).

<table>
<thead>
<tr>
<th>TABLE I</th>
<th>THE STRAIN IN THE WALL OF NATIVE AORTA, ETE, EETE AND SFA ANASTOMOSES AT DIFFERENT LEVELS OF THE INNER PRESSURE</th>
</tr>
</thead>
<tbody>
<tr>
<td>( \epsilon ) (%)</td>
<td>( \epsilon ) (%)</td>
</tr>
<tr>
<td>Native aorta</td>
<td>60 mmHg</td>
</tr>
<tr>
<td>( \pm 9.37 )</td>
<td>( \pm 11.62 )</td>
</tr>
<tr>
<td>SFA</td>
<td>26.41</td>
</tr>
<tr>
<td>( \pm 67.25 )</td>
<td>( \pm 6.29 )</td>
</tr>
<tr>
<td>EETE</td>
<td>10.01</td>
</tr>
<tr>
<td>( \pm 1.59 )</td>
<td>( \pm 1.73 )</td>
</tr>
<tr>
<td>ETE</td>
<td>4.83</td>
</tr>
<tr>
<td>( \pm 1.22 )</td>
<td>( \pm 1.29 )</td>
</tr>
</tbody>
</table>

Maximum strain at inner pressure 220 mmHg was 47.65±15.41 %. The stress of the native aorta at inner pressure 60 mmHg was 45.32±15.29 kPa, at 80 mmHg it was 65.36±24.2 kPa, at 100 mmHg it was 86.31±33.54 kPa (Table II). At inner pressure 220 mmHg the stress was 253.41 ± 95.94 kPa. In cases with anastomosis \textit{end-to-end} (ETE) the relationship between stress and strain was practically linear (Fig. 3). The strain in ETE decreased and at 60 mmHg it was 4.83±1.22 %, at 80 mmHg it was 6.33±1.29 % and at 100 mmHg it was 7.63 ± 1.22 %. Maximum strain at the suture sight at the inner pressure 220 mmHg reached only 15.78±3.09 %. Comparing the strain of native aorta with anastomoses, we came to conclusion that the strain of the anastomosis ETE was much smaller but at the inner pressure 220 mmHg it was twice smaller than in the native aorta.
modulus of elasticity at inner pressure 60-80 mmHg was 683.29±65.87 kPa, but at 100-120 mmHg 1232.79±586.79 kPa. In the cases of SFA modulus of elasticity at the inner pressure 60-80 mmHg was 615.95±50.88 kPa, but at the pressure 100-120 mmHg was 1158.35±127.52 kPa, which is closer to the modulus of elasticity of the native vessel.

The light microscopy after hematoxylin-eosin staining of the aortic wall following the pressurizing up to 220 mmHg in the experimental stand showed oedema, dislocation and disorientation of the elastic fibres.

V.DISCUSION

Despite successful surgical correction and/or balloon angioplasty of the aortic coarctation complications such as development of hypertension and recoarctation are common. Aorta becomes enclosed in a scar tissue and elastic properties of the aortic wall in these segments are not preserved. Besides that this may be also related to further extension of the ductal tissue into the aortic wall and the loss of natural aortic elasticity which are responsible for blood pressure abnormalities [17]-[19]. Arterial stiffness persists despite satisfactory correction of the coarctation and it is shown to be the risk factor of such cardio-vascular events as primary coronary events, stroke and mortality. Clinical trials have shown that even normotensive patients after coarctation repair have markedly increased left ventricle mass as a sequel of increased aortic stiffness and pulse wave velocities, decreased central aortic dispensability and compliance [20], [21]. Our data show significant difference between the biomechanical properties of the native aorta and different anastomoses used for the surgical correction of coarctation with the strain of the surgically corrected aorta much smaller. The modulus of elasticity of the native aorta increases with the increase of the inner pressure but this increase is most limited in the cases of ETE anastomosis. The data are acquired from in vitro study, so the limitation is the difference between experimental results and real patients. We compared these data to the clinical outcomes of the patients operated due to coarctation in The Clinic for Pediatric Cardiology and Cardiac Surgery of University Hospital for Children Riga, Latvia within the first year of life in the period of time from January 1, 2000 to

\[
\begin{array}{|c|c|c|c|c|}
\hline
\text{Pressure (mmHg)} & \sigma (kPa) & \sigma (kPa) & \sigma (kPa) & \sigma (kPa) \\
\hline
60 & 45.32 & 65.36 & 86.31 & 108.04 \\
80 & 51.10 & 65.09 & 78.35 & \\
100 & 54.44 & 70.11 & 86.66 & \\
\hline
\end{array}
\]

\[
\begin{array}{|c|c|c|c|}
\hline
\text{Pressure (mmHg)} & \text{SFA} & \text{EETE} & \text{ETE} & \\
\hline
60 & 35.99 & 39.32 & 36.15 & \\
80 & 51.10 & 54.44 & 49.52 & \\
100 & 65.09 & 70.11 & 63.41 & \\
\hline
\end{array}
\]

\[
\begin{array}{|c|c|c|c|}
\hline
\text{Pressure (mmHg)} & \text{Native aorta} & \text{SFA} & \text{EETE} & \text{ETE} \\
\hline
60 & 516.08 & 615.95 & 683.29 & 902.39 \\
80 & 704.02 & 798.46 & 932.63 & 1138.16 \\
100 & 967.45 & 1158.35 & 1232.79 & 1261.35 \\
\hline
\end{array}
\]

Fig. 3 The relationship between the pressure and strain; 1-anastomosis end-to-end (ETE), 2 – extended anastomosis end-to-end (EETE), 3 –subclavian flap aortoplasty (SFA), 4 –native aorta

In the cases of subclavian flap aortoplasty the strain at inner pressure 60 mmHg was 26.41±67.25 %, at 80 mmHg was 28.87±6.29 %, but at 100 mmHg was 30.62±6.26 %. Maximum strain at inner pressure 220 mmHg reached 37.73±7.86 %, which is the closest to the strain of the native aorta. In the cases of EETE the strain at inner pressure 60 mmHg was 10.01±1.59 %, at 80 mmHg was 12.25±1.73 %, and at 100 mmHg was 14.06±2.05 %. The modulus of elasticity at inner pressure 60-80 mmHg was closer to the modulus of elasticity of the native aorta at the inner pressure 100-120 mmHg. The results showed that in the cases of ETE stiffness practically does not change with the changes of inner pressure that might affect haemodynamics. In the cases of EETE
December 31, 2010 and followed-up to December 31, 2011 (n=60, follow-up period 18-112 months) [22]. Our experimental data showed the biomechanical properties of SFA the closest to the native aorta. These clinical data are consistent with the outcomes of these experimental results and showed the relieve of the maximum pressure gradient in descending aorta detected by echocardiography early post operation in ETE 25.53+/+9.4 mmHg (95% CI 11-37), ETEE 17.64+/+4.5 mmHg (95% CI 13-22) and SFA 15.95+/+6.6 mmHg (95% CI 6-34). Long term follow-up data showed no statistically significant recoarctation rate differences between the groups of different techniques: 18% in ETE group, 26% in SFA and 25% in ETEE group (p>0.05). The priority of SFA might be less tension on the suture lines, no circular scars and the use of autologous tissue with the growth potential but the drawback is the need to scarify the left subclavian artery, therefore most centres prefer ETEE in cases of infantile coarctation with isthmus and sometimes transverse aortic arch hypoplasia [5], [7]-[9]. The choice of a surgical approach is usually made by the surgeon on the basis of individual abnormalities in the shape of the arch. In the age group included in our study physiological blood pressure limits up to 90th percentile according to the age specific percentile table are up to 74/50 mmHg in infants 1-3 days old, 89/58 mmHg at the age 2-3 weeks, but 106/71 mmHg at the age 1-5 months [23]. The differences between the biomechanical properties of the native aorta and the aorta following surgical correction were less prominent within the range of physiological arterial pressure for the age and more obvious with the increase of inner pressure above the physiological limits. That is consistent with the findings of elevated arterial pressure during physical activities in otherwise normotensive patients following successful coarctation repair.

VI. CONCLUSION

The results of the experiments showed that neonatal and infantile aorta has significant strain of the wall which provide physiologic hemodynamics. Even successful surgical correction means a significant loss of elastic properties and the increasing of stiffness of the arterial wall which is less evident within the range of physiological pressures for the age. The anastomoses ETEE and SFA showed elastic properties closer to native aorta in comparison with ETE.

REFERENCES