Treatment of Paper and Pulp Mill Effluent by Coagulation

Pradeep Kumar, Tjoon Tow Teng, Shri Chand, and Kailas L. Wasewar

Abstract—The pulp and paper mill effluent is one of the high polluting effluent amongst the effluents obtained from polluting industries. All the available methods for treatment of pulp and paper mill effluent have certain drawbacks. The coagulation is one of the cheapest process for treatment of various organic effluents. Thus, the removal of chemical oxygen demand (COD) and colour of paper mill effluent is studied using coagulation process. The batch coagulation process was performed using various coagulants like: aluminium chloride, poly aluminium chloride and copper sulphate. The initial pH of the effluent (Coagulation pH) has tremendous effect on COD and colour removal. Poly aluminium chloride (PAC) as coagulant reduced COD to 84 % and 92 % of colour was removed at an optimum pH 5 and coagulant dose of 8 ml l\(^{-1}\). With aluminium chloride at an optimum pH \(= 4\) and coagulant dose of 5 g l\(^{-1}\), 74 % COD and 86 % colour removal were observed. The results using copper sulphate as coagulant (a less commercial coagulant) were encouraging. At an optimum pH 6 and mass loading of 5 g l\(^{-1}\), 76 % COD reduction and 78 % colour reduction were obtained. It was also observed that after addition of coagulant, the pH of the effluent decreases. The decrease in pH was highest for AlCl\(_3\), which was followed by PAC and CuSO\(_4\). Significant amount of COD reductions was obtained by coagulation process. Since the coagulation process is the first stage for treatment of effluent and some of the coagulant cations usually remain in the treated effluents. Thus, cation like copper may be one of the good catalyst for second stage of treatment like wet oxidation. The copper has been found to be good oxidation catalyst then iron and aluminium.

Keywords—Aluminium based coagulants, Coagulation, Copper, PAC, Pulp and paper mill effluent, Wastewater treatment

I. INTRODUCTION

INTEGRATED pulp and paper mill generates wastewater with very high BOD and COD, toxic substances, recalcitrant organics, pH, turbidity, high temperature and intense color. The colouring body present in the wastewater from pulp and paper mill is organic in nature and is comprised of wood extractives, tannin resins, synthetic dyes, lignin and its degradation products formed by the action of chlorine on lignin [1]. Paper industry consumes large amount of water (about 250-300 m\(^3\) per tones of paper) and generate an equal amount of wastewater [2]. Black liquor (originating from the chemical pulping stage) contains lignin, carbohydrates, organic acids, sulfur compounds, phenolic compounds, terpenes, resin, etc. Pulp and paper effluents contain a number of compounds which are harmful to receiving waters and are inhibitory or recalcitrant to biological treatment. Conventional treatment processes like chemical pre-treatment [3], lagooning [4], and activated sludge treatment [5, 6] are not adequate to meet the regulatory effluent standards for being discharged into sewers. Therefore, the pulp and paper industry has to use tertiary polishing stage to meet the effluent discharge standards.

Several treatment methods are in use in large mills including physico-chemical and biological. The biological treatment is also not very effective in reducing colour [7], although BOD and COD reduction has been found to be satisfactory. However, lignin and its derivatives show high stability to degradation [8, 9]. Wet air oxidation (catalytic and non-catalytic) has been found to reduce BOD, COD and colour to a large extent. However, the energy requirement and the use of high pressure reactors and associated equipment make the wet air oxidation of large volume of wastewater uneconomical. Chemical precipitation (and/or coagulation) using alum, ferric chloride, lime, ferrous sulphate and poly aluminium chloride (PAC) have been studied extensively [10-14]. Although economical, in comparison to other methods, the precipitation method has other associated drawbacks like dewatering and disposal of the generated sludge.

Primary treatment methods like physical, chemical and thermal pre-treatment may be followed by anaerobic, aerobic and enzymatic treatment methods to remove the residual organics, which is largely degradable. Coagulation/ flocculation can, however, be used as an effective primary treatment method to remove much of the toxicity, colour, and COD (and BOD). This treatment will make the secondary treatment cost effective as well as efficient in the removal of residual toxic organic compounds and colour.

It has been seen that most of the reported research work used aluminium, ferrous salts and its polyelectrolyte for the coagulation/ flocculation process, to remove the toxic organic materials from the wastewater in order to make it amenable to secondary treatment, like wet air oxidation (WO) or biological treatment. The present paper deals the COD and colour removal of pulp and paper mill effluent using aluminium salts like aluminium chloride and polyaluminium chloride and also the new coagulant cuprous sulphate. As per our knowledge, no one has studied the CuSO\(_4\).5H\(_2\)O as coagulant. Since, pH has tremendous effect in coagulation process, hence in present studies, at constant mass loading, the initial pH is varied using alkali and acid, which saves the coagulants doses. This type
of studies has not been found in past literatures. They have
maintained the initial pH of wastewater and added the
coa gulants, which causes less COD reductions even at high
mass loading of coagulants.

II. MATERIALS AND METHODS

A. Effluent

Black liquor was obtained from a local integrated kraft pulp
and paper mill. This liquor was having a COD of about 7 x
10^5 mg l^-1. Synthetic wastewater was prepared by diluting this
black liquor with distilled water to obtain a COD value of
about 7000 mg l^-1. The average characteristics of the synthetic
wastewater are presented in Table I.

TABLE I
CHARACTERISTICS OF DILUTED BLACK LIQUOR

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Chemical oxygen demand (COD) (mg l^-1)</td>
<td>7000</td>
</tr>
<tr>
<td>Biochemical oxygen demand (BOD) (mg l^-1)</td>
<td>1400</td>
</tr>
<tr>
<td>pH</td>
<td>10.45</td>
</tr>
<tr>
<td>Total solids (TS) (mg l^-1)</td>
<td>7240</td>
</tr>
<tr>
<td>Total dissolved solids (TDS) (mg l^-1)</td>
<td>6680</td>
</tr>
<tr>
<td>Total suspended solids (TSS) (mg l^-1)</td>
<td>560</td>
</tr>
<tr>
<td>Conductivity (µmhos cm^-1)</td>
<td>51760</td>
</tr>
<tr>
<td>Color</td>
<td>Dark brown</td>
</tr>
</tbody>
</table>

B. Coagulants and Chemicals

Analytical reagent (AR) grade chemicals have been used for
the analysis of the parameters during coagulation/ flocculation
studies. Laboratory reagent (LR) grade AlCl_3 and analytical
grade (AR) CuSO_4.5H_2O obtained from s. d. fine Chemicals
Ltd., Mumbai (India) and the commercial grade aqueous
solution of polyaluminium chloride (PAC) was obtained from
M/s Jubilant Organosys Limited, Gajraula, India, which were
used in the experiments. The characteristics of the PAC, AlCl_3
and CuSO_4.5H_2O are given in Table 2. The X-ray diffraction
pattern of the solid PAC sample supplied by another company
was performed earlier by Srivastava et al. [12]. The major
components identified were AlCl_3, Al_2O_3, Al_2SiO_5 and
3Al_2O_3.2SiO_2. The scanning electron micrographs of the PAC
at 100x and 1000x magnification showed small particulate
structure in a matrix and also the larger porous particles
embedded into it [12].

TABLE II
CHARACTERISTICS OF PAC, AlCl_3, CuSO_4.5H_2O

<table>
<thead>
<tr>
<th>Characteristics</th>
<th>PAC</th>
<th>AlCl_3</th>
<th>CuSO_4.5H_2O</th>
</tr>
</thead>
<tbody>
<tr>
<td>Appearance</td>
<td>Pale yellow liquid</td>
<td>Pale yellow solid</td>
<td>Dark sky blue</td>
</tr>
<tr>
<td>Specific gravity</td>
<td>1.486</td>
<td>-----</td>
<td>-----</td>
</tr>
<tr>
<td>Al/Cu content</td>
<td>3.33 mg/ml</td>
<td>0.202 mg/mg</td>
<td>0.2545 mg/mg</td>
</tr>
<tr>
<td>pH of 1% solution</td>
<td>3.39 (V/V)</td>
<td>1.96 (w/v)</td>
<td>4.30</td>
</tr>
<tr>
<td>Sulphate</td>
<td>Nil</td>
<td>0.01%</td>
<td>38.476%</td>
</tr>
</tbody>
</table>

C. Experimental method

0.20 dm^3 of pulp and paper mill effluent was taken in a 0.50
dm^3 glass beaker. The pH of the effluent was noted. A known
amount of the coagulant was added to the effluent and the
initial pH (pH_0) was adjusted by adding aqueous NaOH (1 M)
or H_2SO_4 (1 M) solution, than it is flash-mixed for 5 minutes
by a stirrer and, thereafter, slowly mixed for 15 minutes. The
effluent sample was then taken in a glass cylinder and kept
quesient for 6 h. The supernatant liquor was centrifuged
and analysed for its COD and colour value. These steps were
repeated at different dosages of the coagulant. Thus, the
experiments were planned with the objectives: (i) Optimizing
pH for maximum COD removal (ii)To get optimum coagulant
dose at optimum pH for maximum COD removal.

An experimental detail of the coagulation study is given in
Fig 1.

![Flow chart showing the steps for coagulation studies](image)

D. Analytical Methods

The treated samples were centrifuged in a Remi Centrifuge
(Model R 24, Remi Instruments, Mumbai, India). The COD of
the effluent was determined by dichromate open reflux
method as per standard method [15]. The colour of the initial
and final effluent after the treatment was measured at a
wavelength of 263 nm using UV/VIS spectrophotometer
(Model Lambda 35 Perkin Elmer, Switzerland).

III. RESULTS AND DISCUSSION

The pulp and paper mill effluent contains reduced
carbohydrates, lignin and resins, etc. The carbohydrates have
mainly carboxylic and hydroxyl functional groups. The
biorefractory molecule – lignin contains phenolic, hydroxyl
and benzoylic hydroxyl groups. When aluminium chloride
(AlCl_3), PAC and Copper sulphate are dissolved in water, the
metal ions hydrate and hydrolyse to form monomeric and
polymeric species: M(OH), MOH^2+, M_2(OH)^4+, M(OH)_4^2−,
M(OH)_2(s) and M(OH)_4 etc. At low pH (pH < 7), both Al^3+
and Cu remain in the solution, and form precipitates of CuOH
or Al(OH)₃, as the pH is increased or as the coagulant dosage is raised [16]. The general form of hydrolysis reaction of trivalent metals is represented as [17]

\[ xM^{3+} + yH_2O \rightarrow M_x(OH)_y^{(3x-y)+} + yH^+ \]

The metal hydroxide polymers have amorphous structure, very large surface area, and possess positive charge [18]. These hydroxides are hydrophobic, causing them to adsorb onto the organic anionic particle surface and become insoluble [16, 17]. Copper and aluminium cations tend to associate and complex with a number of functional groups and ligands, especially with polar molecules and with oxygen containing functional groups like hydroxyl, phenolic and carboxylic groups [19-21]. The local negative charge of these groups is neutralised by the Al and Cu cations, resulting in colloid destabilization and precipitation of the metal (cations) – organics (anions) complexes. This phenomenon induces sweep flocculation and the adsorption and bridging enhancement of both particulate organics and inorganic solids to form large, amorphous flocs [22]. The precipitation is enhanced as the pH is lowered in the presence of multivalent cations.

**E. Effect of pH on COD and Color Removal**

Figure 2 and 3 show the effect of pH on the COD reduction as well as colour removal of the wastewater having an initial COD value of 7000 mg l⁻¹ at ambient temperature (25 °C) using different coagulants. The coagulant mass loading was kept uniformed as 5 g l⁻¹ for AlCl₃ and CuSO₄·5H₂O and 5 ml l⁻¹ for PAC. The runs were taken at different initial pH (pH₀) values, i.e., at 2.0, 4.0, 5.0, 6.0, 7.0 and 8.0. The supernatant was then decanted off and its COD was measured. For aluminium chloride, the COD reduction was found considerable at pH₀ ≤ 5 and maximum at the pH of 4.0 resulting in a COD reduction of 74 %. At pH₀ > 5, the COD reduction is found to decrease. For the coagulation by PAC, the maximum COD reduction (70 %) is noted at pH₀ = 5. After increasing or decreasing initial pH from 5, the COD reduction was found to decrease in both the cases. Similar COD reduction phenomena was noted for coagulation of biocatalyst effluent of an alcohol distillery plant using AlCl₃ and PAC [23]. For 5 g l⁻¹ of CuSO₄, the COD reduction was increased from pH₀ 1.5 to 6.0, then decreased as pH₀ was increased from 6 to 8. The maximum 80 % COD reduction was obtained using this coagulant at pH₀ 6. CuSO₄·5H₂O showed better results (80 % COD reduction) being the low molal feed (5.1 mM Cu ≈ 5g/l CuSO₄·5H₂O) than AlCl₃ (74 % COD reduction) at higher molal feed (7.57 mM ≈ 5g/l AlCl₃). This may be due to presence of greater unfield orbital in copper than aluminium. The anionic compounds of wastewater act as good reagents and electron donor to the Cu.

The variation in colour reduction was also studied, it was found to be in order of COD reduction for all the coagulant (Fig 3). The decolourization is expressed as the percent decrease in the absorbance of the biocatalyst effluent sample from the untreated sample at \( \lambda = 263 \text{ nm} \). The optimum colour reduction is found to be 86 %, 78 % and 82 % for AlCl₃, CuSO₄·5H₂O and PAC treated effluent at their optimum pH₀: pH₀ = 4 for AlCl₃, pH₀ = 5 for PAC and pH₀ = 6 for CuSO₄·5H₂O. For the coagulation with CuSO₄·5H₂O, the COD reduction is highest in comparison to AlCl₃ and PAC (Fig. 2), however, the colour removal is lower than these coagulants, which may be due to the colour of CuSO₄·5H₂O itself. The CuSO₄·5H₂O produces blue colour, when it is dissolved in water.
coagulant. Thus, it may be concluded that the COD and colour reduction of pulp and paper effluent is a strongly dependent on the pH₀ value.

F. Effect of Mass Loading on COD and Colour Removal

The addition of different coagulants in the effluent and its flash mixing, creates proper coagulation condition. Gentle mixing thereafter initiates floc formation, complexation and adsorption of the organics resulting in the precipitation and settling of the insoluble solids.

For different coagulants, the effect of mass loading on the COD reduction of the synthetic wastewater (COD₀ = 7,000 mg l⁻¹) was studied at ambient temperature of 25 °C at their optimum pH₀ (Fig 4). The coagulant mass loading was varied from 1 to 9 g l⁻¹ for AlCl₃ and CuSO₄.5H₂O, and 1 to 9 ml l⁻¹ for PAC. From the figure, it is observed that as PAC coagulant dose is increased, the COD reduction is increased till 8 ml l⁻¹ coagulant dose, after which, the COD reduction is almost unchanged. Thus, the 8 ml l⁻¹ of PAC dose is optimum, resulting in 84 % COD reduction. For CuSO₄.5H₂O coagulant, the COD reduction has been found to increase till 5 g l⁻¹ dose, giving maximum COD reduction of 76 %. After increase in coagulant loading, the COD reduction decreases, indicating, 5 g l⁻¹ as optimum dose to CuSO₄.5H₂O. The decrease in COD reduction at higher dose of copper sulphate may be due to excess amount of cations (Cu⁺) causing the repletion in itself, providing less chances for coordinating copper cations of coagulant with anions present in wastewater. For AlCl₃ coagulant, the COD reduction has increased considerably till its loading of 5 g l⁻¹, giving ~ 74 % COD reduction. After an increase in its loading, the COD reduction increased marginally till 7 g l⁻¹ and beyond which, the COD reduction has decreased.

G. Variation in pH of Effluent by Adding Coagulants

The addition of metal ions in wastewater decreases its pH. The decrease in pH is proportional to amount of metal ions. Fig 6 shows variation of pH with dose of coagulants. The decrease in pH is less for dose of 8 ml PAC in comparison to dose of 5 g AlCl₃. It shows low amount of aluminium content in PAC than AlCl₃. Having the low amount of aluminium in PAC than AlCl₃, it gives high COD and colour reductions. It may be due to polymeric structure of the PAC. The multivalent Al cations of PAC coordinate with the anions present in pulp and paper mill effluent. And result in complexation. The gel structure of PAC also enmeshes the organics present in wastewater. Thus the complexation (and consequent precipitation) and the capture of the organics in the gel are responsible for the higher COD/colour reduction by PAC as compared to those obtained with AlCl₃ and CuSO₄.5H₂O.

The colour reduction at optimum pH of coagulation for different coagulants is presented in Fig 5. For optimum mass loading of CuSO₄.5H₂O (5 g l⁻¹), AlCl₃ (5 g l⁻¹) and PAC (8 ml l⁻¹) at optimum pH₀, the colour reductions are found to be 75 %, 88 % and 92 %, respectively.
The effect of different coagulants, such as, PAC, aluminium chloride and copper sulfate on the COD and colour reduction are presented in Fig 7. From the figure, it may be seen that at their optimum dose, 8 ml l⁻¹ for PAC, and 5 g l⁻¹ for CuSO₄·5H₂O and AlCl₃, the COD reduction is maximum (84 %) for PAC which is followed by CuSO₄·5H₂O (76 %) and AlCl₃ (74 %).

The corresponding colour reductions 92 % for PAC, followed by 86 % for AlCl₃, and 78 % for CuSO₄·5H₂O.

The colour compounds present in the paper mill effluent are negatively charged, which get neutralized from the positively charged coagulant and remove the colour of the wastewater. The colour reduction increases up to a breakpoint, after which it starts decreasing due to increase in the coagulant concentration.

### Table III

<table>
<thead>
<tr>
<th>Coagulants</th>
<th>Concentration</th>
<th>Effluent type</th>
<th>Initial TC/COD Parameter (%) removal</th>
</tr>
</thead>
<tbody>
<tr>
<td>Alum</td>
<td>100 mg l⁻¹</td>
<td>Paper machine</td>
<td>COD 96</td>
</tr>
<tr>
<td>Ferric chloride</td>
<td>10 g l⁻¹</td>
<td>BCTMP/TMP</td>
<td>COD 50 Colour 80 Turbidity 90</td>
</tr>
<tr>
<td>Aluminium chloride</td>
<td>10 g l⁻¹</td>
<td>BCTMP/TMP</td>
<td>Colour 90</td>
</tr>
<tr>
<td>B+ Alum</td>
<td>100+300 mg l⁻¹</td>
<td>Paper and pulp</td>
<td>Colour About 91</td>
</tr>
<tr>
<td>CaB + Alum</td>
<td>1000+300 mg l⁻¹</td>
<td>industry wastewater</td>
<td>Colour About 91</td>
</tr>
<tr>
<td>Br5 + Alum</td>
<td>400+300 mg l⁻¹</td>
<td></td>
<td>Colour About 95</td>
</tr>
<tr>
<td>BS + Alum</td>
<td>1000+ 300 mg l⁻¹</td>
<td></td>
<td>Colour About 93</td>
</tr>
<tr>
<td>PAC (Poly aluminium chloride)</td>
<td>3 g l⁻¹</td>
<td>Alkaline black liquor</td>
<td>COD 80 Colour 90 CO2 61.4</td>
</tr>
<tr>
<td>Copper sulphate</td>
<td>5 g l⁻¹</td>
<td>Black liquor</td>
<td>COD 80 Colour 90 CO2 61.4</td>
</tr>
<tr>
<td>PAC</td>
<td>8 ml l⁻¹</td>
<td>Black liquor</td>
<td>COD 80 Colour 90 CO2 61.4</td>
</tr>
</tbody>
</table>

### A. Comparison of Results

Results obtained by other researchers to treat paper mill effluent have been compared in the Table 3, showing, the % COD and % colour removal along with the effluent type, coagulant type and their concentration. Stephenson et al. (1996) [10] obtained 90% colour removal using 10 g l⁻¹ dose of aluminium chloride. The dose is quite high in comparison to 86.30% colour removal at 5 g l⁻¹ dose in present work. Copper sulphate is used by Garg et al. for thermal precipitation of pulp and paper mill effluent [13], who have observed 61.4% COD removal. The better result (74% COD removal) in present work (using CuSO₄ coagulant) may be due to different process used by Garg et al. They have performed thermal precipitation reaction at 95 ⁰C. In the present work, the coagulation is performed at room temperature.
temperature ~ 25 °C. Poly aluminium chloride has given better result as 82.85% COD removal and 91.81% colour removal, which is better to that obtained by Srivastava et al. [12].

IV. CONCLUSIONS

The pH of effluent has found to tremendous effect on COD and colour removal by coagulation process. The pH 4, 5 and 6 were optimum values for AlCl₃, CuSO₄ and PAC respectively.

The maximum COD and colour removal of 84 % and 92 % respectively were obtained using PAC (8 ml l⁻¹) as compared to 72 % and 84 % with aluminium chloride (5 g l⁻¹) and 74 % and 76 % with copper sulphate (5 g l⁻¹) at their optimum pH.

After addition of coagulants, the pH of the effluent had decreased. The decrease in pH was maximum for AlCl₃ which was followed by PAC and CuSO₄.

The addition of catalyst followed by pH adjustment to its optimum value can save the coagulant dose considerably.

PAC is found to be a better coagulant in comparison to other two coagulants. However, copper sulphate may also be considered as a better prospective coagulant because the Cu content in supernatant works as a good catalyst for wet oxidation in the next stage of treatment by wet oxidation.

REFERENCES