Simulation and Realization of a Battery Charge Regulator

B. Nasri, and M. Bensaada

Abstract—We present a simulation and realization of a battery charge regulator (BCR) in microsatellite earth observation. The tests were performed on battery pack 12 volt, capacity 24 Ah and the solar array open circuit voltage of 100 volt and optimum power of about 250 watt. The battery charge is made by solar module. The principle is to adapt the output voltage of the solar module to the battery by using the technique of pulse width modulation (PWM). Among the different techniques of charge battery, we opted for the technique of the controller ON/OFF is a standard technique and simple, it’s easy to be board executed validation will be made by simulation "Proteus Isis Professional software". The circuit and the program of this prototype are based on the PIC16F877 microcontroller, a serial interface connecting a PC is also realized, to view and save data and graphics in real time, for visualization of data and graphs we develop an interface tool "visual basic.net (VB)".

Keywords—Battery Charge Regulator, Batteries, Buck converter, Power System, Power Conditioning, Power Distribution, Solar arrays.

I. INTRODUCTION

THE Controller design for any subsystem in the spatial domain needs knowledge about system behavior. Usually this involves a mathematical description of the relation among inputs to the process, state variables, and output. This description in the form of mathematical equations which describe behavior of the system (process) is called model of the system.

The DC/DC converters are widely used in regulated switch mode DC power supplies. The input of these converters is an unregulated DC voltage, which is obtained by PV array and therefore it will be fluctuated due to changes in radiation and temperature. In these converters the output voltage regulation in the DC/DC converter is achieved by constantly adjusting the amount of energy absorbed from the source and that injected into the load, which is in turn controlled by the relative durations of the absorption and injection intervals.

These two basic processes of energy absorption and injection constitute a switching cycle. Intuitively speaking, if

\[
\begin{align*}
\frac{dv}{dt} &= \frac{1}{C} \left( i_L - \frac{v_0}{R} \right) \\
\frac{di}{dt} &= \frac{1}{L} \left( V_{in} - v_0 \right)
\end{align*}
\]

the energy storage capacity of the converter is too small or the switching period is relatively too long, then the converter would have transmitted all the stored energy to the load before the next cycle begins. This introduces an idling period immediately following the injection interval, during which the converter is not performing any specific task [1, 2, 3]. We find the block diagram of controller battery charge.

A. Converter Modeling

The buck converter with ideal switching devices will be considered here which is operating with the switching period of T and duty cycle D Fig. 2, [4]. The state equations corresponding to the converter in continuous conduction mode (CCM) can be easily understood by applying Kirchhoff’s voltage law on the loop containing the inductor and Kirchhoff’s current law on the node with the capacitor branch connected to it. When the ideal switch is ON, the dynamics of the inductor current \( i_L(t) \) and the capacitor voltage \( V_C(t) \) are given by:

\[
\begin{align*}
\frac{di}{dt} &= \frac{1}{L} \left( V_{in} - v_0 \right) \\
\frac{dv}{dt} &= \frac{1}{C} \left( i_L - \frac{v_0}{R} \right)
\end{align*}
\]

and when the switch is OFF are presented by,

\[
\begin{align*}
\frac{di}{dt} &= \frac{1}{L} \left( - v_0 \right) \\
\frac{dv}{dt} &= \frac{1}{C} \left( i_L - \frac{v_0}{R} \right)
\end{align*}
\]
TABLE I
THE VALUES THE BUCK CONVERTER

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Quantity</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Vin</td>
<td>Input Voltage</td>
<td>42V</td>
</tr>
<tr>
<td>Vout</td>
<td>Output Voltage</td>
<td>13V</td>
</tr>
<tr>
<td>D</td>
<td>Duty Cycle</td>
<td>1 - 99%</td>
</tr>
<tr>
<td>F</td>
<td>Switching Frequency</td>
<td>100KHz</td>
</tr>
<tr>
<td>L</td>
<td>Inductor</td>
<td>125mH</td>
</tr>
<tr>
<td>C</td>
<td>Capacitor</td>
<td>250µF</td>
</tr>
<tr>
<td>R</td>
<td>Load Resistor</td>
<td>15Ω</td>
</tr>
</tbody>
</table>

B. Software Development of the Control Regulator

The organization associated with the proposed control algorithm is described in Fig. 3. During charging, the IRF740 (mosfet) bloc load behaves like a short circuit and the whole current of the solar array is used for battery charging. Once the Voltage reaches the regulation voltage (Voltage Regulation Setpoint) [2], the microcontroller will act on the mosfet the charging current and maintain consequently the battery voltage. This operation allows the regulator to protect the battery against overcharging. The battery is enabled again when the voltage drops below the value (Voltage Regulation Reconnect Setpoint) [5].

The charge controller conceived also protects the battery against deep discharge. Once the nominal battery voltage and rated capacity, reaches a value to low (Low Voltage Disconnect Setpoint) [6], where the discharge current is assumed to be negative, the microcontroller will act on the IRF740 the bloc limiting discharge to disconnect the battery usage and stop his defense accordingly when the battery has taken a correct voltage level (Low Voltage reconnect Setpoint) [7].

C. Hardware Implementation

A detailed block diagram of the proposed system is shown in Fig. 5. The buck-type DC/DC converter is designed according to the system power capability requirements, as analyzed in [8]. The control unit in Fig. 4 consists of microcontroller 16F877A and interface circuits required to lead the battery voltage, and current signals to the microcontroller. The microcontroller on-chip 8-bit pulse width modulation (PWM) generator output drives the DC/DC
converter, according to the battery charging algorithm analyzed below. The control unit has its power supply from the battery, which is charged by the DC/DC converter. The battery voltage is measured by means of a voltage divider interfaced to an op-amp-based voltage-follower, and a Hall-effect based sensor is used to measure the battery current [9]. The components used are given in Table II.

![Fig. 4 Detailed diagram of the proposed system](image)

**Fig. 4 Detailed diagram of the proposed system**

**TABLE II**

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Voltage divider</td>
<td>TL082</td>
</tr>
<tr>
<td>Low pass filter</td>
<td>TL082</td>
</tr>
<tr>
<td>Current divider</td>
<td>LA100P</td>
</tr>
<tr>
<td>Optocoupler</td>
<td>4N35</td>
</tr>
<tr>
<td>Driver</td>
<td>4049</td>
</tr>
<tr>
<td>Voltage divider</td>
<td>TL082</td>
</tr>
<tr>
<td>Low pass filter</td>
<td>15Ω</td>
</tr>
</tbody>
</table>

D. Preliminary Result Obtained

A software program in visual basic.net for windows was developed for the microcontroller sent data via the RS232 serial ports. Information received in the PC is displayed numerically and graphically.

![Fig. 5 Battery Voltage](image)

**Fig. 5 Battery Voltage**

II. CONCLUSION

Objective was the realization of a charge controller of battery acid-plomb in a photovoltaic system. The prototype is a card based 16f877 microcontroller and a power card consists of a buck DC-DC. The ON / OFF algorithm was used to charge the battery when the end of life equipment in the satellite can patch the threshold voltage, the initial values of the battery in the microcontroller. The experimental results ensure the maximization of the energy transferred to the battery, with a long life and less time to charge the battery.

REFERENCES


