Thermo-mechanical deformation behavior of functionally graded rectangular plates subjected to various boundary conditions and loadings

Mohammad Talha and B N Singh

Abstract—This paper deals with the thermo-mechanical deformation behavior of shear deformable functionally graded ceramic-metal (FGM) plates. Theoretical formulations are based on higher order shear deformation theory with a considerable amendment in the transverse displacement using finite element method (FEM). The mechanical properties of the plate are assumed to be temperature-dependent and graded in the thickness direction according to a power-law distribution in terms of the volume fractions of the constituents. The temperature field is supposed to be a uniform distribution over the plate surface (XY plane) and varied in the thickness direction only. The fundamental equations for the FGM plates are obtained using variational approach by considering traction free boundary conditions on the top and bottom faces of the plate. A C⁰ continuous isoparametric Lagrangian finite element with thirteen degrees of freedom per node have been employed to accomplish the results. Convergence and comparison studies have been performed to demonstrate the efficiency of the present model. The numerical results are obtained for different thickness ratios, aspect ratios, volume fraction index and temperature rise with different loading and boundary conditions. Numerical results for the FGM plates are provided in dimensionless tabular and graphical forms. The results proclaim that the temperature field and the gradient in the material properties have significant role on the thermo-mechanical deformation behavior of the FGM plates.

Keywords—Functionally graded material, higher order shear deformation theory, finite element method, independent field variables.

I. INTRODUCTION

An advanced composite materials known as functionally graded material (FGM) have received an appreciable consideration in structural engineering design, especially when the materials are subjected to extremely high thermal loading. The material property of the FGM can be tailored to accomplish the specific demands in different engineering utilization to achieve the advantage of the properties of individual material. This is possible due to the material composition of the FGM changes sequentially in a preferred direction. The applicability of this material is that it eliminates the interface problem due to proficient and continuous change of material properties from one surface to the other [1] [2]. The thermo-mechanical deformation of FGM structures have attracted the attention of many researchers in the past few years in different engineering applications which include design of aerospace structures, heat engine components and nuclear power plants etc.

The assessment of thermo-mechanical deformation behavior of functionally graded plate structures considerably depends on the plate model kinematics. A number of plate theories are available to analyze the deformations of composite plates. The foremost constraint of using the classical Kirchhoff plate theory (CLPT) is that it ignores transverse shear effects and consequently provides reasonable results for relatively thin plates [24]. To abstain the said complication, an earlier attempts were made by Reissner [3] and Mindlin [4]. However, a shear-correction factor is needed to eliminate the problem of a constant transverse shear stress distribution. This correction factor was obtained by comparing the results with an exact elasticity solution and generally it depends on various parameters such as boundary conditions, geometric parameters, and loading conditions. This classical Kirchhoff plate theory seems to be unreliable for analysis of the FGM plates, in which volume fractions of two or more constituent varies smoothly and continuously as a function of position in a pre-defined specifications. Due to the continuous variation of material properties in a preferred direction, the first order shear deformation theory (FSDT) and higher order shear deformation theory (HSDT) may be efficiently utilized in the analysis. However, many HSDT kinematics were proposed, notable among them are [5], [6], [7], [8]. The higher order theories assumes the in-plane displacements as a cubic expression of the thickness coordinate and the out-of-plane displacement to be constant.

Several authors have used FSDT and HSDT kinematics to analyze the deformation characteristics of FGM plates. For example, Reddy [9] presented the mathematical formulation in conjunction with finite element model, based on third order shear deformation theory for static and dynamic analysis of the FGM plates. Abrate [10] analyzed the problems of free vibrations, buckling, and static deflections of the FGM plates using CLPT, FSDT, and HSDT kinematics. Sang and Hwan [11] investigated vibration and thermal postbuckling behaviors of the functionally graded plates with nonlinear temperature distribution. Lanhe [12] applied FSDT kinematics to derive the equilibrium and stability equations of a moderately thick FGM rectangular plate under thermal loads, with two types of thermal loading, uniform temperature rise and gradient through the thickness. Saidi and Jomehzadeh [13] presented a new analytical method for bending-stretching analysis of thick FGM plates based on the FSDT or Mindlin plate theory. Sheng and Wang [14] investigated the effect of thermal load on vibration, buckling and dynamic stability of FGM cylindrical shells em-
bedded in an elastic medium, based on FSDT by considering rotary inertia and the transverse shear strains. Ferreira et al. [15] used FSDT and multiquadric radial basis functions to analyze the static deformations of a simply supported FGM plates. They derived the effective properties of the composite either by rule of mixtures or by the Mori-Tanaka scheme. Yang and Shen [16] analyzed the free and forced vibration analyses for initially stressed FGM plates in thermal environment with temperature dependent material properties. The formulations are based on Reddy’s higher order shear deformation theory which includes the thermal effects due to uniform temperature variation. Qian et al. [17] analyzed the static and dynamic response of a simply supported square FGM plate by using compatible higher order shear and normal deformable plate theory and a meshless Petrov-Galerkin method. Efraim and Eisenberger [18] derived the equations of motion for annular plates by employing FSDT which includes the effect of shear deformations to accomplish vibration frequencies and modes for various combinations of boundary conditions.

Naei et al. [19] presented the buckling analysis of radially-loaded circular FGM plate with variable thickness. The finite-element method is used to determine the critical buckling load and the effects of thickness variation and Poisson’s ratio are investigated by calculating the buckling load. Navazi and Hadadpour [20] analytically investigated the zero-thickness stability margins of FGM panels in thermal environment by employing piston theory of aeroelasticity to model quasi-steady aerodynamic loading. Reddy and Cheng [21] studied the harmonic vibration problem of FGM plates in terms of transfer matrix by means of a three-dimensional asymptotic approach. Nguyen et al. [22] proposed the FSDT model for modelling structures made of FGM materials using energy equivalence methods. Liew et al. [23] presented a continuum three dimensional Ritz formulation for the vibration analysis of homogeneous thick rectangular plate with arbitrary combinations of boundary conditions.

With the enhanced utility of these materials in many diversified engineering applications, it is essential to know the thermo-mechanical deformation behavior of functionally graded ceramic-metal plates under various loading and boundary conditions. Considering the above said viewpoint in mind, the objective of this investigation is to present a higher order shear deformation theory with a cubically varying in-plane displacements over the entire thickness and quadratically varying transverse displacement to ensure the effects of normal strain and its derivative in calculation of transverse shear strains. The material properties of the FGM plates are graded continuously in the thickness direction. The variation of the properties follows according to a simple power-law distribution in terms of the volume fractions of the constituent. The implementation of this theory is executed by using a suitable C6 continuous isoparametric finite element, and the governing equations are obtained using the variational approach. The thermo-mechanical deformations behavior of the FGM plates are examined for different thickness ratios, the aspect ratios, temperature rise, for different volume fraction indices, loading and boundary conditions. The present accomplished results are compared with those available in the literature. The obtained results are presented in the form of tables and figures to show the parametric effect such as material properties, thickness ratios, aspect ratios, temperature fields, the loading and boundary conditions, which can be treated as a benchmark for further advanced research. These furnished results are significant from the point of view in the designing of thermal barrier materials.

II. PROBLEM FORMULATION

A. Governing equations

A schematic diagram of the problem studied and the rectangular cartesian coordinate system used describe the thermo-mechanical deformations of the FGM plate are shown in Fig. 1. It is assumed that the material properties of FGM plate varies in the thickness direction only, such that the top surface \( (z = h/2) \) of the plate is ceramic rich, whereas the bottom surface \( (z = -h/2) \) is metal rich. The effective material properties at an arbitrary point within the structural domain, like Young’s modulus \( E \), Poisson’s ratio \( \nu \), mass density \( \rho \), thermal expansion coefficient \( \alpha \), of the functionally graded plate are the effective material properties \( P \). These properties are position dependent and can be expressed as,

\[
P = P_1V_l(z) + P_0V_b(z)
\]

where \( P_1 \) and \( P_0 \) represents the temperature dependent properties of the top and bottom faces of the plate, respectively, and can be expressed as a function of temperature [25].

\[
P = P_0(P_{-1}T^{-1} + 1 + P_1T^1 + P_2T^2 + P_3T^3)
\]

where \( P_0 \), \( P_{-1} \), \( P_1 \), \( P_2 \), and \( P_3 \) are the coefficients of temperature \( T(K) \) and are exclusive to the constituent materials. \( V_l(z) \) and \( V_b(z) \) are defined as the volume fractions of the constituent of the top and bottom faces of the plates, respectively, and are related by

\[
V_l(z) + V_b(z) = 1
\]

The effective properties of functionally graded material

Fig. 1. Schematic diagram and dimensions of the plate.

are obtained according to a simple power-law. The volume fractions of the constituent of the top surface of the plate follows a simple power-law as

\[
V_l(z) = \left( \frac{2z + h}{2h} \right)^n
\]

where \( n \) is the non-negative volume fraction index which prescribes the material variation profile through the thickness
of the plate and may be adjusted to obtain the optimum distribution of the constituent material. It is ascertained that the effective Young’s modulus \( E \) and thermal expansion coefficient \( \alpha \) are the temperature dependent. However, the mass density \( \rho \) and the thermal conductivity \( \kappa \) are independent of the temperature. Poisson’s ratio \( \nu \) is assumed to be constant as it weakly depends on the temperature changes. From Eqs. (1) and (4), the effective material properties with two constituents for graded plates can be expressed as,

\[
E(z, T) = E(T) - E_0(T) \left( \frac{2z+h}{2h} \right)^n + E_0(T) \\
\alpha(z, T) = \left[ \alpha(T) - \alpha_0(T) \right] \left( \frac{2z+h}{2h} \right)^n + \alpha_0(T) \\
\rho(z) = (\rho_1 - \rho_0) \left( \frac{2z+h}{2h} \right)^n + \rho_0 \\
\kappa(z) = (\kappa_1 - \kappa_0) \left( \frac{2z+h}{2h} \right)^n + \kappa_0
\]

Throughout the analysis the temperature field is applied in the thickness direction only and one-dimensional temperature field is assumed to be constant in the \( XY \) plane of the plate. In order to obtain the temperature distribution along the thickness a steady-state heat transfer equation is solved, and can be represented as,

\[
- \frac{d}{dz} \left[ \kappa(z) \frac{dT}{dz} \right] = 0
\]

This equation is solved by prescribing boundary condition of \( T = T_1 \) at \( z = h/2 \) and \( T = T_0 \) at \( z = -h/2 \). It can be seen from Eqs. (5) and (7) that \( E(T), \alpha(z) \) and \( \alpha_0(z) \) are all functions of position and temperature dependent. The linear thermo-mechanical constitutive relations are,

\[
\begin{bmatrix}
\sigma_{xx} \\
\sigma_{yy} \\
\sigma_{zz} \\
\sigma_{xy} \\
\sigma_{yz} \\
\sigma_{xz}
\end{bmatrix} = \begin{bmatrix}
Q_{11} & Q_{12} & Q_{13} & 0 & 0 & 0 \\
Q_{12} & Q_{22} & Q_{23} & 0 & 0 & 0 \\
Q_{13} & Q_{23} & Q_{33} & 0 & 0 & 0 \\
0 & 0 & 0 & Q_{44} & 0 & 0 \\
0 & 0 & 0 & 0 & Q_{55} & 0 \\
0 & 0 & 0 & 0 & 0 & Q_{66}
\end{bmatrix} \begin{bmatrix}
\varepsilon_{xx} \\
\varepsilon_{yy} \\
\varepsilon_{zz} \\
\gamma_{xy} \\
\gamma_{xz} \\
\gamma_{yz}
\end{bmatrix} + \begin{bmatrix}
0 \\
0 \\
0 \\
\alpha(x, T) \\
0 \\
0
\end{bmatrix}
\]

where \( \sigma_{xx}, \sigma_{yy}, \sigma_{zz}, \sigma_{xy}, \sigma_{xz}, \sigma_{yz} \) are the stress components, \( \varepsilon_{xx}, \varepsilon_{yy}, \varepsilon_{zz}, \varepsilon_{xy}, \varepsilon_{xz}, \varepsilon_{yz} \) are the strain components. \( Q_{ij} \) are the stiffness coefficients, with \( Q_{11} = Q_{22} = Q_{33} = E(x, y)(1 - \nu^2)/(1 - 2\nu), Q_{12} = Q_{13} = Q_{23} = E(x, y)(1 + \nu)/(1 - 2\nu), Q_{44} = Q_{55} = Q_{66} = 2\nu E(x, y)/(1 - \nu) \).

The linear strains corresponding to the displacements \((\bar{u}, \bar{v}, \bar{w})\) at any point along the \((x,y,z)\) axes, respectively can be expressed as,

\[
\begin{bmatrix}
\varepsilon_{xx} \\
\varepsilon_{yy} \\
\varepsilon_{zz} \\
\gamma_{yz} \\
\gamma_{xz} \\
\gamma_{yx}
\end{bmatrix} = \begin{bmatrix}
\frac{\partial \bar{u}}{\partial x} \\
0 \\
0 \\
0 \\
0 \\
0
\end{bmatrix} \\
\begin{bmatrix}
\frac{\partial \bar{v}}{\partial y} \\
0 \\
0 \\
0 \\
0 \\
0
\end{bmatrix} \\
\begin{bmatrix}
\frac{\partial \bar{w}}{\partial z} \\
0 \\
0 \\
0 \\
0 \\
0
\end{bmatrix}
\]

To incorporate the transverse shear effects in proposed HSDT kinematics, the displacement field is expressed in terms of mid-plane displacements \( u, v \) and \( w \) perpendicular to mid-plane \( z \), and the rotation of the normal \( \psi_x \) and \( \psi_y \) about the \( y \) and \( x \)-axis, respectively. In order to ensure the field variables to be continuous within the element for \( C^0 \) finite element modelling, the out of plane derivatives are considered as independent degrees of freedom, see [27] and the resulting modified displacement field is represented as,

\[
\begin{bmatrix}
u \quad \psi \quad \psi \quad \psi \quad \psi \quad \psi
\end{bmatrix} = \begin{bmatrix}
u(n, \psi_x, \psi_y, \psi_z, \alpha_x, \alpha_y, \alpha_z, \beta_x, \beta_y, \beta_z, \theta_x, \theta_y)
\end{bmatrix}^T
\]

where, \( \begin{bmatrix} q \end{bmatrix} \) is named as displacement vector.

The strain vector terms in terms of mid-plane strain vector can be written as,

\[
\begin{bmatrix}
\varepsilon_{xx} \\
\varepsilon_{yy} \\
\varepsilon_{zz} \\
\gamma_{yz} \\
\gamma_{xz} \\
\gamma_{yx}
\end{bmatrix} = \begin{bmatrix}
\varepsilon_0 \\
\varepsilon_0^y \\
\varepsilon_0^z \\
\gamma_{y} \\
\gamma_{x} \\
\gamma_{x}
\end{bmatrix} + \begin{bmatrix}
k_1 \\
k_2 \\
k_3 \\
k_4 \\
k_5 \\
k_6
\end{bmatrix} + \begin{bmatrix}
z^2 \\
z^2 \\
z^2 \\
z^2 \\
z^2 \\
z^2
\end{bmatrix}
\]

where,

\[
\begin{align*}
\varepsilon_0^1 &= \frac{\partial \bar{u}}{\partial y} + \frac{\partial \bar{v}}{\partial x} \\
\varepsilon_0^2 &= \frac{\partial \bar{u}}{\partial x} + \frac{\partial \bar{v}}{\partial y} \\
\varepsilon_0^3 &= \frac{\partial \bar{w}}{\partial y} \\
\varepsilon_0^4 &= \frac{\partial \bar{w}}{\partial x} \\
\varepsilon_0^5 &= \frac{\partial \bar{w}}{\partial z} \\
\varepsilon_0^6 &= \frac{\partial \bar{w}}{\partial x} + \frac{\partial \bar{w}}{\partial y} + \frac{\partial \bar{w}}{\partial z}
\end{align*}
\]

\[
\begin{align*}
k_1 &= \frac{\partial \bar{u}}{\partial y} - \alpha_y, \\
k_2 &= \frac{\partial \bar{u}}{\partial x} + \alpha_x, \\
k_3 &= \frac{\partial \bar{v}}{\partial y} - \alpha_y, \\
k_4 &= \frac{\partial \bar{v}}{\partial x} + \alpha_x, \\
k_5 &= \frac{\partial \bar{w}}{\partial y} - \beta_y, \\
k_6 &= \frac{\partial \bar{w}}{\partial x} + \beta_x
\end{align*}
\]

In the above expressions, the terms having superscripts ‘0’, ‘1’ and ‘2’ – ‘3’ are membrane, curvature and higher order strain terms, respectively. The modulus \( E \), thermal expansion

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coefficient \( \alpha \) and the elastic coefficients \( Q_{ij} \) vary through the plate thickness according to the Eqs.(4) and (5). The total in-plane force resultants, moments and higher order moments produced due to temperature rise are defined as, 
\[
\{ N^T \} = \left\{ \begin{array}{ccc} N_{x z} \\
N_{y z} \\
N_{z y} \end{array} \right\} = \int_{-h/2}^{h/2} \left\{ \begin{array}{ccc} \sigma_{x x} \\
\sigma_{y y} \\
\sigma_{z y} \end{array} \right\} dz, \\
\{ M^T \} = \left\{ \begin{array}{ccc} M_{x x} \\
M_{y y} \\
M_{z y} \end{array} \right\} = \int_{-h/2}^{h/2} \left\{ \begin{array}{ccc} \sigma_{x x} \\
\sigma_{y y} \\
\sigma_{z y} \end{array} \right\} z dz \\
\{ P^T \} = \left\{ \begin{array}{ccc} P_{x x} \\
P_{y y} \\
P_{z y} \end{array} \right\} = \int_{-h/2}^{h/2} \left\{ \begin{array}{ccc} \sigma_{x x} \\
\sigma_{y y} \\
\sigma_{z y} \end{array} \right\} z^3 dz \\
\]

and
\[
\{ q \} = \sum_{i=1}^{NN} N_i \{ q \}_i; \quad x = \sum_{i=1}^{NN} N_i x_i; \quad y = \sum_{i=1}^{NN} N_i y_i 
\]

where, 
\[
\{ q \} = \left[ \begin{array}{c} \Delta u \\
\Delta v \\
\Delta w \\
\end{array} \right]
\]

As the plate is exposed to thermal environment, and subsequently produces in-plane stress resultants \( (N_{x z}, N_{y z}, N_{z y}) \). Therefore, the work done by the in-plane forces produced due to temperature change produces out of plane displacement \( w' \) by using small deformation theory as,
\[
W_{th} = \frac{1}{2} \int_A \left\{ \begin{array}{ccc} w, x \\
w, y \\
N_{x z} N_{y z} N_{z y} \\
N_{x z} N_{y z} N_{z y} \\
N_{x z} N_{y z} N_{z y} \end{array} \right\} \left\{ \begin{array}{ccc} w, x \\
w, y \end{array} \right\} dA 
\]

B. Strain energy
The strain energy of the FGM plate is given by,
\[
U = \frac{1}{2} \int_V \{ \varepsilon \}^T \{ \sigma \} dV
\]

The global displacement field model as given by Eq.(8) may be represented as,
\[
\{ u \} = [ \tilde{N} ] \{ q \} 
\]

where \( \{ q \} \) is as defined in Eq. (10) and the function of thickness co-ordinate \( [ \tilde{N} ] \) is defined as,
\[
[ \tilde{N} ] = \left[ \begin{array}{cccccccccccccccc} 1 & 0 & 0 & f_1(z) & 0 & 0 & f_3(z) & 0 & f_4(z) & 0 \\
0 & 1 & 0 & f_2(z) & 0 & 0 & f_3(z) & 0 & f_4(z) & 0 \\
0 & 0 & 1 & 0 & 0 & f_3(z) & 0 & f_6(z) & 0 & 0 \\
0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
\end{array} \right]
\]

C. Work done due to external transverse load
The external work done due to the distributed transverse static load \( p_0(x, y) \) can be expressed as,
\[
W_{ext} = \frac{1}{2} \int_A p_0(x, y) w dA. 
\]

III. SOLUTION METHODOLOGY
A. Finite element model
A nine noded isoparametric element is employed for finite element modeling. In the FEM the domain is discretized into a set of finite elements. Over each of the elements, the displacement vector and element geometry of the model is expressed by,
\[
\{ q \} = \sum_{i=1}^{NN} N_i \{ q \}_i; \quad x = \sum_{i=1}^{NN} N_i x_i; \quad y = \sum_{i=1}^{NN} N_i y_i 
\]

where \( N_i \) is the interpolation function (shape function) for the \( i \)th node, \( \{ q \}_i \) is the vector of unknown displacements for the \( i \)th node, \( NN \) is the number of nodes per element and \( x_i \) and \( y_i \) are Cartesian coordinate of the \( i \)th node.

1) Strain energy of the plate: The strain energy of the FGM plate is given by,
\[
U = \sum_{e=1}^{NE} U^{(e)} 
\]

here \( NE \) is number of elements used for meshing the plate \( U^{(e)} \) is the elemental strain energy which can be obtained using Eqs. (16) and (20) and expressed as,
\[
U = \frac{1}{2} \sum_{e=1}^{NE} \{ q \}^{T(e)} [ K ]^{(e)} \{ q \}^{(e)} 
\]

where \( [ K ]^{(e)} \) and \( \{ q \}^{(e)} \) are defined as linear stiffness matrix and displacement vector for the \( e \)th element, respectively. Using finite element model (Eq.(15)), Eq.(20) may also be written as,
\[
W_{th} = \sum_{e=1}^{NE} W^{(e)} = \sum_{e=1}^{NE} \{ q \}^{T(e)} [ K ]^{(e)} \{ q \}^{(e)} dA. 
\]

where, \( [ K ]^{(e)} \) is defined as the elemental geometric stiffness matrix for the \( e \)th element.

2) Work done due to external transverse load: The work done by external mechanical load \( p_0(x, y) \) is given by
\[
V = \frac{1}{2} \int_A p_0(x, y) w dA. 
\]

Using the finite element notation model, Eq. (19) may be written as,
\[
V = \sum_{e=1}^{NE} V^{(e)} 
\]

where, \( V^{(e)} = \int_A \{ q \}^{T(e)} [ P ]^{(e)} dA = \{ q \}^{(e)T} [ P ]^{(e)} \)

with \( [ P ]^{(e)} = (00000000000000000)T^{(e)} \)

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B. Governing Equation

The governing equation for thermo-mechanical deformations of the FGM plate can be derived using variational principle as:

$$[K] \{q\} = \{F\}$$  \hspace{1cm} (26)

with, $[K] = [K + \gamma K_c] - [K_g]$, $\gamma \in \mathbb{R}^+$.

where, $[K]$, $[K_c]$, $[K_g]$, $\{q\}$, and $\{F\}$ are global linear stiffness matrix, global linear stiffness matrix arises due to constraints, global geometric stiffness matrix due to thermal load, global displacement vector, and force vector, respectively.

IV. NUMERICAL EXAMPLES AND DISCUSSION

The numerical results for thermo-mechanical deformations of the FGM plates are computed using the proposed mathematical model in conjunction with FEM. A computer programme has been developed in MATLAB 7.5.0 (R2007b) environment. The validation and efficacy of the proposed algorithm is examined by comparing the results with those available in the literature. A nine noded Lagrange isoparametric element, 13 degrees of freedom (DOFs) per node for the present HSDT model has been used for discretizing the plate. For the computation of results full integration schemes (3x3) are used for thick plates and selective integration schemes (2x2) for thin plates. Table 1 shows the temperature dependent properties of the FGM constituents which have been used for the computation of the results throughout the study, unless specified otherwise. Fig. 2 shows the volume fraction of the ceramic phase through the dimensionless thickness. It is assumed that the materials are perfectly elastic throughout the deformation.

The boundary conditions used in the present analysis are as follows:

Simply supported:(SSSS)

$$u_0 = w_0 = \psi_y = \alpha_x = \alpha_z = \beta_y = \theta_x = 0, \text{ at } x = 0 \text{ and } a.$$  $$v_0 = w_0 = \psi_x = \psi_y = \alpha_x = \alpha_z = \beta_y = \beta_x = \theta_x = \theta_y = 0, \text{ at } y = 0 \text{ and } b.$$

Clamped:(CCCC)

$$u_0 = v_0 = w_0 = \psi_x = \psi_y = \psi_z = \alpha_x = \alpha_y = \alpha_z = \beta_x = \beta_y = \theta_x = \theta_y = 0, \text{ at } x = 0, \alpha \text{ and } y = 0, b.$$  $$v_0 \neq x \neq w_0 \neq y \neq z \neq \alpha \neq \alpha \neq \alpha \neq \beta \neq \beta \neq \beta \neq \beta \neq \beta \neq \beta \neq \beta \neq \beta \neq \beta \neq \beta \neq \beta$$

Simply supported-clamped: (SCSC)

$$u_0 = w_0 = \psi_y = \alpha_x = \alpha_z = \beta_y = \theta_x = 0, \text{ at } x = 0 \text{ and } y = 0.$$  $$v_0 = w_0 = \psi_x = \psi_y = \psi_z = \alpha_x = \alpha_y = \alpha_z = \beta_x = \beta_y = \theta_x = \theta_y = 0, \text{ at } x = 0 \text{ and } y = 0.$$  $$w_0 = \psi_x = \psi_y = \psi_z = \alpha_x = \alpha_y = \alpha_z = \beta_x = \beta_y = \theta_x = \theta_y = 0, \text{ at } x = a \text{ and } y = b.$$
TABLE II

<table>
<thead>
<tr>
<th>Mesh size</th>
<th>Volume fraction index, n</th>
<th>ceramic</th>
<th>0.5</th>
<th>1</th>
<th>2</th>
<th>metal</th>
</tr>
</thead>
<tbody>
<tr>
<td>Present(2 x 2)</td>
<td>0.0239</td>
<td>0.0300</td>
<td>0.0330</td>
<td>0.0358</td>
<td>0.0500</td>
<td></td>
</tr>
<tr>
<td>Present(3 x 3)</td>
<td>0.0274</td>
<td>0.0345</td>
<td>0.0381</td>
<td>0.0414</td>
<td>0.0573</td>
<td></td>
</tr>
<tr>
<td>Present(4 x 4)</td>
<td>0.0218</td>
<td>0.0264</td>
<td>0.0303</td>
<td>0.0329</td>
<td>0.0455</td>
<td></td>
</tr>
<tr>
<td>Present(5 x 5)</td>
<td>0.0201</td>
<td>0.0256</td>
<td>0.0287</td>
<td>0.0312</td>
<td>0.0431</td>
<td></td>
</tr>
<tr>
<td>Present(6 x 6)</td>
<td>0.0201</td>
<td>0.0256</td>
<td>0.0286</td>
<td>0.0312</td>
<td>0.0431</td>
<td></td>
</tr>
<tr>
<td>Ferreira et al. [15]</td>
<td>0.0205</td>
<td>0.0262</td>
<td>0.0294</td>
<td>0.0323</td>
<td>0.0443</td>
<td></td>
</tr>
<tr>
<td>% Difference</td>
<td>1.99</td>
<td>2.34</td>
<td>2.43</td>
<td>3.52</td>
<td>2.78</td>
<td></td>
</tr>
</tbody>
</table>

Example 2. In this example we consider the static deformations of thick FGM plate made of Aluminium (Al) and Silicon Carbide (SiC) by using higher-order shear and normal deformable plate theory and meshless local Petrov-Galerkin method given by Qian et al. [17]. The top surface of the plate is assumed to be ceramic-rich, whereas the bottom surface is metal rich. The thickness to side ratio (a/h) is taken as 0.2. The top surface of the plate is loaded by a normal pressure obtained by \( q_0 \sin \pi x/a \sin \pi y/a \) and the bottom surface of the plate is assumed to be traction free. The material properties for Al and SiC are as follows:

- Al: \( E_t = 70 \text{ GPa}, \nu_t = 0.3, \rho_t = 2702 \text{ kg/m}^3 \),
- SiC: \( E_t = 427 \text{ GPa}, \nu_t = 0.17, \rho_t = 3100 \text{ kg/m}^3 \).

In this example the transverse displacement \( w \) and thickness coordinate \( z \) have been non-dimensionalized as: \( \bar{w} = \frac{100E_0h^3}{E_t a^4 q_0} w, \bar{z} = \frac{z}{h} \). The plate is simply supported (SSSS) at all its edges. The non-dimensional centre deflections with volume fraction index \( n \) along with the figure layout are preferred as used in Ref. [17] for direct comparison. Again, a good agreement is observed between the two results as shown in Fig.3.

These two comparison studies show that the present results matches well with the established one.

V. PARAMETRIC STUDIES

Based on the established approach and analyses of foregoing sections it is acknowledged that (5 x 5) mesh has been found to give good convergence for the FGM plates as mentioned earlier. These have been used for accomplishing the results, unless it is stated otherwise.

Table 3 shows the nondimensional central deflection of \( \text{ZrO}_2/\text{Ti-6Al-4V} \) square FGM plate in thermal environment.

Table 4 represents the nondimensional central deflection of \( \text{ZrO}_2/\text{Ti-6Al-4V} \) square FGM plate subjected to a uniform lat-
The side to thickness ratio \(\frac{a}{h}\) is taken as 10 and the uniform lateral pressure is given by \(q\frac{a}{bh}\); load parameter, \(P = p_0a^2/\left(E_ih^2\right)\); and thickness coordinate, \(\bar{z} = z/h\). The side to thickness ratio is \(\frac{a}{h}\) is taken as 10 and the uniform lateral pressure is ranging from \(q_0 = 10\) to \(q_0 = 100\). The nondimensional central deflection increases as the volume fraction index \(n\) increases in all type of boundary conditions considered here. This is expected, because a larger volume fraction index means that the plate has a smaller ceramic component, and that its stiffness is thus reduced. The variation of nondimensional central deflection of \(\text{ZrO}_2/\text{Ti}-6\text{Al}-4\text{V} \) rectangular FGM plate subjected to a uniform lateral pressure combined with a temperature rise \(\Delta T = 100K\) is described in Tables 5 and 6 for \(a/h = 5\) and 10, respectively. The thermo-mechanical deformation characteristics shown in these two tables are similar to those in tables 3 and 4. It is also evident that the rectangular plates deflected more than the square plates.

Table 7 shows the nondimensional central deflection of \(\text{ZrO}_2/\text{Ti}-6\text{Al}-4\text{V} \) FGM plate subjected to a sinusoidal load given by \(q_0\sin\pi x/a\sin\pi y/a\) combined with a temperature rise \(\Delta T = 100K\) for various boundary conditions considered here. The side to thickness ratio \(\frac{a}{h}\) is 5 and the plate aspect ratio \(\frac{b}{a}\) is taken as 1 and 2, respectively. The transverse displacement \(w\) and thickness coordinate \(z\) have been nondimensionalized as: \(\bar{w} = \frac{100E_ih^3}{P}\frac{E_i}{E_f}\frac{h^2}{w}, \bar{z} = \frac{z}{h}\). The mass density and thermal conductivity are: \(\rho = 2370\text{ kg/m}^3, \kappa = 1.8\text{W/mK for}\ \text{ZrO}_2, \rho = 4429\text{ kg/m}^3, \kappa = 7.82\text{W/mK for}\ \text{Ti}-6\text{Al}-4\text{V}\). Young’s modulus and thermal expansion coefficient of these materials are assumed to be temperature-dependent as given in Table 1. The load parameter \(p_0\) is taken as unity. It is noticed that in the case of square plate (b/a=1) the maximum center deflection is found for simply supported (SSSS) boundary conditions and least for clamped (CCCC) boundary condition, whereas, for rectangular plate (b/a=2) maximum is found for clamped-free (CCCF) and minimum for clamped (CCCC) boundary condition. The volume fraction index \(n\) increases in all type of boundary conditions considered here, as expected.

Table 8 represents the variation of nondimensional central deflection of \(\text{ZrO}_2/\text{Ti}-6\text{Al}-4\text{V} \) rectangular (b/a=1) and rectangular (b/a=2) FGM plates, respectively, subjected to a uniform lateral pressure combined with a temperature rise \(\Delta T = 100K\). The volume fraction index \(n\), and side to thickness ratio \(\frac{a}{h}\), is taken as 1 and 10, respectively, The load parameter \(p_0\)

### Table IV

<table>
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<th>(n)</th>
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<th>CCCC</th>
<th>CSCC</th>
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### Table VI

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### Table VII

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International Scholarly and Scientific Research & Innovation 5(9) 2011 | 1906 | scholar.waset.org/1999.8/7850
TABLE VII

EFFECT OF VOLUME FRACTION INDEX \( n \) ON NONDIMENSIONAL CENTRAL DEFLECTION OF ZRO_{2}/Ti-6Al-4V SQUARE (b = a) AND RECTANGULAR (b = 2a) FGM PLATE (A/H=5) SUBJECTED TO SINUSOIDAL LOAD IN THERMAL ENVIRONMENT.

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varies from 25 to 250. As the present formulation is based on the linear variation of strain fields, hence load Verses deflection pattern is linear. It is also seen that the plates with intermediate material properties have intermediate value of deflection. The minimum deflection is observed for clamped (CCCC) and maximum value is observed for clamped-free (CFCF) boundary conditions for both square and rectangular plates.

Fig. 3. Effect of temperature rise on bending behavior of square Si\(_3\)N\(_4\)/SUS304 plates subjected to uniform pressure and temperature change (\(a/h=10, n=1\)).

Fig. 3 shows the effect of the temperature rise on the nondimensional center deflection for plate made of Si\(_3\)N\(_4\)/SUS304 plates with different combination of boundary conditions. The temperature varies from 100 to 1000 K. The side to thickness ratio, \(a/h\)=10 and the volume fraction index, \(n\) is taken as unity. The top surface of the plate is ceramic rich, whereas the bottom surface is metal rich. A uniformly distributed load is applied on the top of the plate with loading parameter \(p_0=10\). It can be seen that the nondimensional deflection increases as the temperature goes up. This is because the Young’s modulus getting weaker when the temperature goes up. Hence, the weaker Young’s modulus results in the higher deflection. The lowest and highest deflection is found for clamped (CCCC) and clamped-free (CFCF) boundary conditions, respectively.

Fig. 4. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si\(_3\)N\(_4\)/SUS304 square plate (\(a/h=5\) with clamped (CCCC) boundary condition in thermal environment.

Fig. 5. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si\(_3\)N\(_4\)/SUS304 square plate (\(a/h=5\) with clamped-free (CFCF) boundary condition in thermal environment.

Fig. 6. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si\(_3\)N\(_4\)/SUS304 square plate (\(a/h=5\) with hinged (CHCH) boundary condition in thermal environment.
Fig. 7. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si$_3$N$_4$/SUS304 square plate ($a/h=5$) with hinged (HHHH) boundary condition in thermal environment.

Fig. 8. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si$_3$N$_4$/SUS304 square plate ($a/h=5$) with simply supported-clamped (SCSC) boundary condition in thermal environment.

Fig. 9. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si$_3$N$_4$/SUS304 square plate ($a/h=5$) with simply supported (SSSS) boundary condition in thermal environment.

Fig. 10. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si$_3$N$_4$/SUS304 square plate ($a/h=10$) with clamped (CCCC) boundary condition in thermal environment.

Fig. 11. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si$_3$N$_4$/SUS304 square plate ($a/h=10$) with clamped-free (CFCF) boundary condition in thermal environment.

Fig. 12. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si$_3$N$_4$/SUS304 square plate ($a/h=10$) with hinged (CHCH) boundary condition in thermal environment.
TABLE VIII
NONDIMENSIONAL CENTRAL DEFLECTION OF ZrO$_2$/Ti-6Al-4V SQUARE
($b = a$) AND RECTANGULAR ($b = 2a$) FGM PLATE ($a/h = 10$, $n = 1$)
SUBJECTED TO UNIFORM PRESSURE IN THERMAL ENVIRONMENT.

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<th>$p_0$</th>
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Fig. 13. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si$_3$N$_4$/SUS304 square plate ($a/h=10$) with hinged (HHHH) boundary condition in thermal environment.

Fig. 14. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si$_3$N$_4$/SUS304 square plate ($a/h=10$) with simply supported-clamped (SCSC) boundary condition in thermal environment.

Fig. 15. Non-dimensional deflection due to uniformly applied load VS non-dimensional length for Si$_3$N$_4$/SUS304 square plate ($a/h=10$) with simply supported (SSSS) boundary condition in thermal environment.

Fig. 16. Non-dimensional bending behavior of ZrO$_2$/Ti-6Al-4V square plate due to sinusoidal applied load with various boundary conditions in thermal environment ($a/h=5$, $b/a=1$).

Fig. 17. Non-dimensional bending behavior of ZrO$_2$/Ti-6Al-4V rectangular plate due to sinusoidal applied load with various boundary conditions in thermal environment ($a/h=5$, $b/a=2$).
Fig. 18. Effect of volume fraction index $n$ on non-dimensional bending behavior of $\text{Si}_3\text{N}_4$/SUS304 square plate due to uniformly applied load with various boundary conditions in thermal environment ($a/h=5$, $b/a=1$).

Fig. 19. Effect of temperature rise on bending behavior of $\text{ZrO}_2$/Ti-6Al-4V plates subjected to uniform pressure and temperature change ($a/h=2$, $b/a=1$).

Fig. 20. Effect of temperature rise on bending behavior of rectangular $\text{ZrO}_2$/Ti-6Al-4V plates subjected to uniform pressure and temperature change ($a/h=2$, $b/a=2$).

Figs. 4-9 represent the nondimensional deflection VS non-dimensional length with the volume fraction index due to uniformly distributed load ($p_0=10$) along with a uniform temperature rise $\Delta T=100K$ for square $\text{Si}_3\text{N}_4$/ SUS304 plates ($a/h=5$) with different combination of boundary conditions. It is perceived that the nondimensional deflection increases as the volume fraction index $n$ increases, with the trend becoming gentler as $n$ increases. Figs. 10-15 show the nondimensional deflection VS non-dimensional length with the volume fraction index due to uniformly distributed load ($p_0=10$) along with a uniform temperature rise $\Delta T=100K$ for square $\text{Si}_3\text{N}_4$/ SUS304 plates ($a/h=10$) with different combination of boundary conditions. The nondimensional deflection behavior shown in these figures are similar to those in Figs. 4-10. It is noteworthy that when the thermal effect is induced, the mechanical response of graded plate is not necessarily intermediate to that of isotopic metal and the ceramic plate. As shown in Fig. 11, the deflection of the graded plate with $n=4$ is not intermediate with other values of volume fraction index $n$. Figs. 16-17 represent nondimensional bending behavior of square and rectangular $\text{ZrO}_2$/Ti-6Al-4V FGM plates ($a/h=5$), respectively with varying volume fraction index $n$ and under two types of loading conditions. The plates are subjected to sinusoidal load combined with a temperature rise $\Delta T=100K$. It is found that the maximum deflection is observed for simply supported boundary condition (SSSS) for square plate, and consequently in the case of rectangular plate ($b=2a$) same is found for clamped-free (CFCF) boundary condition.

Fig. 18 shows the comparison of the nondimensional deflection, by varying the volume fraction indices, $n$ due to uniformly distributed load ($p_0=10$) along with a temperature rise $\Delta T=100K$ for square $\text{Si}_3\text{N}_4$/SUS304 plates ($a/h=5$) with different combination of boundary conditions. It can be seen that all of the curves that represent the various combinations show the similar behavior with the deflection increases as the volume fraction index $n$ increases, nearly around $n=20$. The deflection is approximately insensitive after $n \geq 20$. Figs. 19-20 represent the effect of the temperature on the nondimensional center deflection for square and rectangular plates, respectively, made up of $\text{ZrO}_2$/Ti-6Al-4V with different combination of boundary conditions. The temperature varies from 100 to 1000 K. The plates are subjected to uniform distributed load with load parameter $p_0=100$. The side to thickness ratio $a/h=10$, and volume fraction index $n=2$. It is found that least deflection is reported for clamped (CCCC) condition and maximum is found in clamped-free (CFCF) type of boundary condition for both square and rectangular plates.

VI. CONCLUDING REMARKS

Thermo-mechanical deformations of functionally graded ceramic-metal plates under various loading and boundary conditions is investigated. The analysis is carried out using the higher order shear deformation theory with an admissible alteration in the transverse displacements in conjunction with finite element models. The systems of algebraic equations are derived using variational approach, and a $C^0$ continuous isoparametric Lagrangian element with 13 DOFs per node is developed and implemented in the said problem. Convergence tests and validation studies have been carried out to inculcate the credibility of the present formulation. The obtained result shows a good agreement with those available in the literature.
It is observed that, when thermal effect is induced, the bending response of the functionally graded plate is not necessarily intermediate to those of the metal and the ceramic plate. This behavior is found to be true irrespective of boundary conditions. The temperature dependent material properties should be taken into account for accurate analysis in high temperature applications. Numerical results for different volume fraction indices, the aspect ratios, the thickness ratios, the temperature rise along with different combinations of the loading and boundary conditions have been presented.

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