Abstract—A basic conceptual study of TCSC device on Simulink is a teaching aid and helps in understanding the rudiments of the topic. This paper thus stems out from basics of TCSC device and analyzes the impedance characteristics and associated single & multi resonance conditions. The Impedance characteristics curve is drawn for different values of inductance in MATLAB using M-files. The study is also helpful in estimating the appropriate inductance and capacitance values which have influence on multi resonance point in TCSC device. The capacitor voltage, line current, thyristor current and capacitor current waveforms are discussed briefly as simulation results. Simulink model of TCSC device is given and corresponding waveforms are analyzed. The subsidiary topics e.g. power oscillation damping, SSR mitigation and transient stability is also brought out.

Keywords—TCSC device, Impedance characteristics, Resonance point, Simulink model

I. INTRODUCTION

RAPID increase in power demand according to forecast made in 17th Electrical power Survey India[11], will rise to peak value of 152746MW by 2011-12, that is more than the double of 75,756 MW, what was required in 2003. This cannot be achieved by installing new power station and erecting more transmission line in the scheduled period of forecast. To meet rising demand of power, FACTS devices are introduced in the transmission line to enhance its power transfer capability; either in series or in shunt. The series compensation are an economic method of improving power transmission capability of the lines [1][2][4]. Note it is not possible to compromise the 2011-12th demand, but meanwhile for installing and erecting periods.

Series compensation will:
- Increase power transmission capability.
- Improve system stability.
- Reduce system losses.
- Improve voltage profile of the lines.
- Optimize power flow between parallel lines.

Thyristor-controlled series capacitors (TCSC) is also a type of series compensator, can provide many benefits for a power system including controlling power flow in the line, damping power oscillations, and mitigating subsynchronous resonance.

World’s first 3 phase [5], 2 X 165 MVAR, TCSC was installed in 1992 in Kayenta substation, Arizona. It raised the transmission capacity of transmission line by 30%, but it was soon realized that the device is also a very effective means for providing damping of electromechanical power oscillations. A third possible application of TCSC emerged from the on site observations that it can provide series compensation without causing the same risk for sub-synchronous resonance (SSR) as a fixed series capacitor. World’s first TCSC for subsynchronous resonance (SSR) mitigation was installed in Stode, Sweden in 1998, by ABB. Specifically this period makes a valiant period for TCSC and makes the researchers to turn on to TCSC

The main purpose of this paper is to furnish a concise study of TCSC in simple way. Section II, brings out the operation of TCSC along with numerical equations. Section III gives an impedance characteristics curve of a TCSC device and specifies the range of inductance and capacitance region. In section IV and V deals, condition for single & multiple resonance points theoretically and evaluate by simulation. Also finds a suitable value of inductance and capacitance. Section VI analyzes the different waveforms in the capacitive region of TCSC with Simulink model. Finally it carries some of additional benefits of TCSC device along with power system in last section.
II. OPERATION OF TCSC [1,2]

The basic operation of TCSC can be easily explained from circuit analysis. It consists of a series compensating capacitor shunted by a Thyristor controlled reactor (TCR). TCR is a variable inductive reactor $X_L$ (figure 2) controlled by firing angle $\alpha$. Here variation of $X_L$ with respect to $\alpha$ is given by

$$X_L(\alpha) = X_L \frac{\pi}{2\alpha - \sin 2\alpha}$$

For the range of 0 to 90 of $\alpha$, $X_L(\alpha)$ start vary from actual reactance $X_L$ to infinity. This controlled reactor is connected across the series capacitor, so that the variable capacitive reactance (figure 3) is possible across the TCSC to modify the transmission line impedance. Effective TCSC reactance $X_{TCSC}$ with respect to $\alpha$ is, [6, 7, 8, 9]

$$X_{TCSC}(\alpha) = -X_C + C_1(2(\pi - \alpha) + \sin(2(\pi - \alpha))) -C_2 \cos^2(\pi - \alpha)(\bar{\omega} \tan(\bar{\omega}(\pi - \alpha)) - \tan(\pi - \alpha))$$

where,

$$X_{LC} = \frac{X_C X_L}{X_C - X_L}$$

$$C_1 = \frac{X_C + X_L}{\pi}$$

$$C_2 = \frac{4X_{LC}^2}{X_L \pi}$$

$$\bar{\omega} = \frac{X_C}{X_L}$$

III. IMPEDANCE CHARACTERISTIC

Figure 4 shows the impedance characteristics curve of a TCSC device. It is drawn between effective restance of TCSC and firing angle $\alpha$ [1, 6, 9, 10]

$$\text{Net reactance of TCR, } X_L(\alpha) \text{ is varied from its minimum value } X_L \text{ to maximum value infinity. Likewise effective reactance of TCSC starts increasing from } X_L(\alpha) \text{ value to till occurrence of parallel resonance condition } X_L(\alpha) = X_C, \text{ theoretically } X_{TCSC} \text{ is infinity. This region is inductive region. Further increasing of } X_L(\alpha) \text{ gives capacitive region, starts decreasing from infinity point to minimum value of capacitive reactance } X_C.$$  

Thus, impedance characteristics of TCSC shows, both capacitive and inductive region are possible though varying firing angle ($\alpha$).

- From $90 < \alpha \leq \alpha_{\text{lim}}$ Inductive region.
- Between $\alpha_{\text{lim}} \leq \alpha \leq \alpha_{\text{clim}}$ Capacitive region
- While selecting inductance, $X_L$ should be sufficiently smaller than that of the capacitor $X_C$ since to get both effective inductive and capacitive reactance across the device.

IV. RELATION BETWEEN THE TCSC RESONANT POINT AND $X_C$ & $X_L$:

From equation 2, it shows the relation between $\omega$ and $X_{TCSS}(\alpha)$. The effective reactance $X_{TCSS}(\alpha)$ would be infinity, when,

$$\bar{\omega}(\pi - \alpha) = (2m \pm 1) \frac{\pi}{2}; \quad (m = 1, 2, 3, ...$$
Or

\[ \alpha_{crt} = \pi - \frac{(2m \pm 1)}{2} \pi \]  

(8)

It is clear from equation (7), that TCSC may appear multiple resonant points in 90° to 180° of firing angle (\(\alpha\)). Note in some paper they refer 0° to 90° of \(\beta\) i.e., conduction angle (\(\beta\)).

\[ \beta = \alpha - \frac{\pi}{2} \]  

(9)

However, only one resonant point, namely one capacitive range and one inductive range, is allowable. Multiple resonant points will reduce the operating range of the TCSC. Thus, some measure as to be taken to ensure only one resonant point between 90° to 180° of \(\alpha\). One obvious way to confine the value of factor 'w' by

\[ w = \frac{X_C}{X_L} < 3 \]  

(10)

V. SIMULATIONS ON M - FILE FOR SINGLE RESONANT POINT IMPEDANCE CHARACTERISTIC CURVE. [6, 7]

For a practical TCSC, the compensation capacitance depends on the requirement of power system in which the TCSC is installed. Once the capacitance of compensation capacitor is specified, the main factor influencing resonant point of TCSC is the reactance \(X_L\). To verify the above theoretical analysis, the simulation has been carried out for \(C = 247.5\mu\)F and for different value of inductances. For \(L = 7.6\)mH and 8.5mH, w is 2.3209 and 2.1946 which is less than 3 is shown in figure 4a and 4b. It shows the single resonant point.

Figure 4c and 4d showing multiple resonant points, for \(L = 2\)mH and 1mH, w is 4.0466 and 6.3983 which violates the equation 10.
VI. ANALYSIS OF THE THYRISTOR CURRENT, CAPACITOR CURRENT AND CAPACITOR VOLTAGE

Figure 5 shows the Simulink model of open loop TCSC device connected in series with the single source transmission line system. For analyzing the Thyristor Current, Capacitor Current and Capacitor Voltage, firing angle pulse are given through pulse generator. To analysis about capacitive mode of TCSC apply the pulse in the region of vernier capacitive region (~160 to 180°). This gives the analysis of waveforms of capacitor voltage, line current, thyristor current and capacitor current of TCSC as shown in figure 6.[6, 8, 9, 10]

Fig. 6 Alpha is 117° for positive and 297° for negative waveforms

VII. BENEFITS OF TCSC DEVICE IN TRANSMISSION LINE

The development and applications of TCSC device adds advantage of not only increasing the transmission line capacity, also improves the power oscillation damping (POD), sub synchronous resonance (SSR) mitigation and transient stability. Research works are mainly focused on improving SSR mitigation, power oscillation damping, and transient stability, which in turn increases the reliability of the system.

A. Damping of power oscillations using TCSC [6,1]

Events in the transmission system like line switching, line faults etc. disturb the steady condition of electric power and angle δ of the generators in the system. During the fault, the sending end generators tend to speed up (accelerate) and angle δ advance while the receiving end generators slow down (decelerate) and angle δ retard. When the fault is cleared, the generators must find a new equilibrium state, where all run with the same speed and with phase angles δ that comply with the new steady state power flow pattern. Due to the inertia of the generators (and participating machines in the load) and the angle versus power characteristics this new equilibrium point will be reached via an oscillation known as “electro-mechanical power oscillation” or simply “power oscillation”. This may lead to system collapse or result in out of synchronism, loss of interconnections and ultimately the inability to supply electric power to the customer. Series compensation is an effective method to damp out the power oscillation.
Essentially the fixed series capacitor does not provide any substantial damping of the subsequent power oscillation, but a controlled series capacitor (TCSC) affords an artificial damping of the power oscillations. During acceleration of generators and angle $\delta$ increases ($d\delta/dt > 0$), the electric power transmitted must be increased to compensate for the excess mechanical input power. On the contrary, when the generators decelerate and angle $\delta$ decreases ($d\delta/dt < 0$), the electric power transmitted must be decreased to balance for the insufficient mechanical input power.

Waveform (figure 7) shows the required variation of the degree of series compensation ($k$), along with undamped and damped oscillation of the angle $\delta$ around the steady state value $\delta_0$ and undamped and damped oscillation of the electric power $P$ around the steady state value $P_0$. From the study, degree of compensation ($k$) is maximum, when $d\delta/dt > 0$, and it is zero when $d\delta/dt < 0$ (if $k$ is maximum, then effective line impedance is minimum, and the electric power transferred is maximum. It is converse, when $k$ is zero). Hence by injecting controlled series reactance in the line, achieving an improved damping of power oscillations.

$$f_c = \frac{1}{2\pi} \sqrt{\frac{1}{LC}} = f \sqrt{\frac{X_C}{X_L}}$$

If the electrical circuit is brought into oscillation by some disturbance, then the subharmonic component of the line current results in a corresponding subharmonic field in the machine which, as it rotates backwards relative to the main field produced an alternating torque on the rotor at the different frequency of $f-f_c$. If this difference frequency coincides with one of the torsional resonances of the turbine-generator set, mechanical torsional oscillation is excited, which, in turn, further excites the electrical resonance. This condition is defined as subsynchronous resonance (SSR).

In 1981 N.G. Hingorani proposed a thyristor controlled damping scheme for series compensators, which has been proven to provide effective SSR mitigation. The basic principle of the NGH damper is to force the voltage of the series capacitor to zero at the end of the each half period if it exceeds the value associated with the fundamental voltage component of the synchronous power frequency.

C. Transient Stability [3, 1]

The relay in the system detects the fault in the transmission system and cause circuit breaker to open at both ends of the line. When the fault is cleared, the circuit breakers are set to reclose automatically after a preset interval of time thus restoring normal operating status of the original circuit. This sequence of breaking/making events constitutes a shock to the power system and is accompanied by transients.

During the period of transient, system may get unstable and loss its reliability. Thus to improve the transient stability margin, the period of persistence of transients has to be minimized. The system locks back into the steady state once the transient dies out.

Discussion of transient stability improvement can be conveniently evaluated by the equal area criterion. The meaning of equal area criterion is explained by two line system and power $P$ versus angle $\delta$ curve, shown in figure 8.
used to select an appropriate value of inductance and MATLAB simulation. In accordance with resonance behavior, resonance condition for different value of inductance by condition of TCSC. This paper inspects the single and multi about the operation, characteristic curve and resonance on TCSC. From that point, this paper precisely explained stability while connecting on the power system.

Figure 9 shows the P Vs δ curve of transmission line with series compensators and explains the substantial increase in the transient stability margin area $A_{\text{margin}}$. Increase in transient stability margin is proportional to the degree of series compensation $k$.

$$P = v^2 \sin \delta / (1-k)$$

Fig. 9 Power Vs Angle curve with series compensation

**REFERENCES**


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